

**HILTI**

TECHNICAL SUPPLEMENT

# Kwik-X Dual Action Anchor

January, 2026



## Kwik-X Dual Action Anchor System

KWIK-X Dual Action Anchor consisting of KHC Capsule and KH-EZ / KH-EZ CRC / KH-EZ SS316 screw anchors

### Features and Benefits

- Combines the high performance of adhesive anchors with the speed and simplicity of screw anchors
- Evaluated by ICC Evaluation Services for cracked concrete and seismic service
- No hole cleaning required for carbon steel anchors – helping save time and eliminating the need for accessories like air compressors and brushes
- OSHA Table 1926.1153 Table 1 compliant installation when installed with Hilti vacuum and DRS system or Hilti SafeSet™ hollow drill bit technology
- Suitable for real jobsite conditions – including water saturated concrete and low installation temperatures
- Screw is fully removable and reusable in the same borehole (one time remove and reuse only, not covered in ESR-5065)
- Immediate loading possible



Hilti KHC Kwik-X capsule



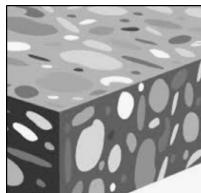
Hilti KH-EZ screw anchor



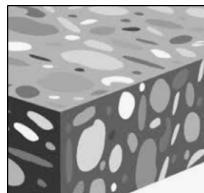
Hilti KH-EZ CRC screw anchor (Mechanically Galvanized)



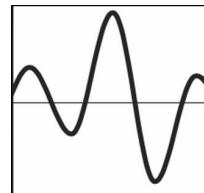
Hilti KH-EZ SS316 screw anchor



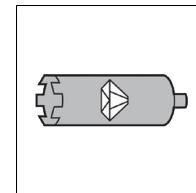
Uncracked concrete



Cracked concrete



Seismic design categories A-F



Diamond core drilling permitted (except for 3/8" Kwik-X SS316 anchors)



Hollow drill bit



PROFIS Engineering Design Software

### Approvals / Listings

<b>ICC-ES (International Code Council)</b>	ESR-5065 in concrete per ACI 318 Ch. 17 / ACI 355.4 / ICC-ES AC308
<b>NSF/ANSI Std 61</b>	Certification for use in potable water
<b>City of Los Angeles</b>	LABC Supplement (within ESR-5065)
<b>Florida Building Code</b>	FBC Supplement (within ESR-5065) w/ HVHZ
<b>U.S. Green Building Council</b>	LEED® Credit 4.1-Low Emitting Materials



## Design Data in Concrete per ACI 318

### ACI 318 Chapter 17 Design

The load tables in this section were developed using the Strength Design parameters and variables of ESR-5065 and the equations within ACI 318 Chapter 17. For more information on ACI 318 Ch. 17 design and the Hilti Simplified Design Tables, refer to sections 3.1.6 and 3.1.8 of the North American Product Technical Guide, Volume 2: Anchor Fastening Technical Guide, Edition 22 (PTG Ed. 22). Data tables from ESR-5065 are not contained in this section but can be found at [www.icc-es.org](http://www.icc-es.org) or at [www.hilti.com](http://www.hilti.com).

Figure 1. Hilti Kwik-X Dual Action Carbon Steel Anchor Installation Conditions

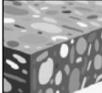
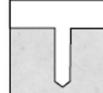
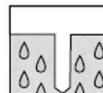
Permissible Base Material	Uncracked concrete	Dry concrete	Permissible Drilling Method
			
Cracked concrete			 Hammer drilling with carbide tipped drill bit
			 Hilti TE-CD or TE-YD hollow drill bit (except 3/8" diameter)
			 Diamond core drill bit

Table 1. Hilti Kwik-X Dual Action with KH-EZ and KH-EZ CRC Screw Anchors Installation Specifications

Design information	Symbol	Units	KH-EZ / KH-EZ CRC anchor diameter (in.)				
			3/8	1/2	5/8	3/4	
Drill hole diameter	$d_o$	in.	3/8	1/2	5/8	3/4	
Minimum fixture hole diameter	$d_f$	in.	1/2	5/8	3/4	7/8	
Nominal embedment <sup>1</sup>	$h_{nom}$	in. (mm)	2-1/2 – 3 (64 – 76)	3 – 4-1/2 (76 – 114)	3 – 4-1/4 (76 – 108)	4-1/4 – 5-1/2 (108 – 140)	3-1/4 – 4-1/2 (83 – 114)
KHC capsule size	-	-	3/8" Small	3/8" Large	1/2" Small	1/2" Large	5/8" Small
Drilled hole depth <sup>2</sup>	Hole condition 1	$h_1$ in. (mm)	$h_{nom} + 5/8$ ( $h_{nom} + 16$ )	$h_{nom} + 3/4$ ( $h_{nom} + 19$ )	$h_{nom} + 1-5/8$ ( $h_{nom} + 41$ )	$h_{nom} + 1-7/8$ ( $h_{nom} + 48$ )	
	Hole condition 2	$h_2$ in. (mm)	$h_{nom} + 3/8$ ( $h_{nom} + 10$ )	$h_{nom} + 3/8$ ( $h_{nom} + 10$ )	$h_{nom} + 3/8$ ( $h_{nom} + 10$ )	$h_{nom} + 3/8$ ( $h_{nom} + 10$ )	
Minimum anchor spacing	$s_{min}$	in. (mm)	3 (76)	3 (76)	4 (102)	4 (102)	
Minimum edge distance	$c_{min}$	in. (mm)	1-1/2 (38)	1-3/4 (44)	1-3/4 (44)	1-3/4 (44)	
Minimum concrete thickness	$h_{min}$	in. (mm)	$h_1 + 1-1/4$ ( $h_1 + 32$ )	$h_1 + 1-1/4$ ( $h_1 + 32$ )	$h_1 + 1-1/4$ ( $h_1 + 32$ )	$h_1 + 1-1/2$ ( $h_1 + 38$ )	

<sup>1</sup>Nominal embedment ( $h_{nom}$ ) = effective embedment ( $h_{ef}$ ).

<sup>2</sup>See Figure 2 for description of drilled hole conditions.

Figure 2. Drilled hole conditions for Kwik-X Dual Action Anchors

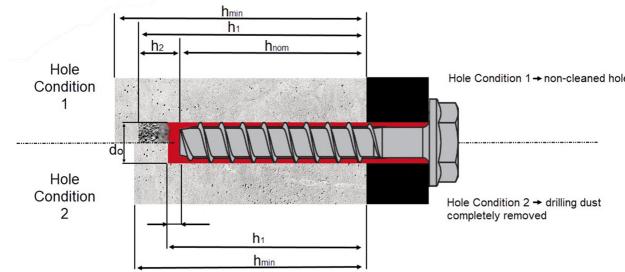


Table 2. Hilti Kwik-X Dual Action Anchor Carbon Steel design strength with concrete / bond failure in uncracked concrete<sup>1,2,3,4,5,6,7,8</sup>

Nominal anchor diameter in. (mm)	Effective embedment in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
		$f_c = 2500$ psi (17.2 MPa) lb (kN)	$f_c = 3000$ psi (20.7 MPa) lb (kN)	$f_c = 4000$ psi (27.6 MPa) lb (kN)	$f_c = 6000$ psi (41.4 MPa) lb (kN)	$f_c = 2500$ psi (17.2 MPa) lb (kN)	$f_c = 3000$ psi (20.7 MPa) lb (kN)	$f_c = 4000$ psi (27.6 MPa) lb (kN)	$f_c = 6000$ psi (41.4 MPa) lb (kN)
3/8	2-1/2 (64)	3,085 (13.7)	3,375 (15.0)	3,900 (17.3)	4,775 (21.2)	6,640 (29.5)	7,275 (32.4)	8,400 (37.4)	10,290 (45.8)
	3-1/4 (83)	4,570 (20.3)	5,005 (22.3)	5,780 (25.7)	6,510 (29.0)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	14,025 (62.4)
	4-1/2 (114)	7,445 (33.1)	7,960 (35.4)	8,380 (37.3)	9,015 (40.1)	16,035 (71.3)	17,140 (76.2)	18,055 (80.3)	19,420 (86.3)
1/2	3 (76)	4,055 (18.0)	4,440 (19.8)	5,125 (22.8)	6,280 (27.9)	8,730 (38.8)	9,565 (42.5)	11,040 (49.1)	13,525 (60.2)
	4-1/4 (108)	6,835 (30.4)	7,485 (33.3)	8,645 (38.5)	10,585 (47.1)	14,720 (65.5)	16,125 (71.7)	18,620 (82.8)	22,805 (101.4)
	5-1/2 (140)	10,060 (44.7)	11,020 (49.0)	12,725 (56.6)	13,970 (62.2)	21,670 (96.4)	23,740 (105.6)	27,410 (121.9)	30,090 (134.0)
5/8	3-1/4 (83)	4,570 (20.3)	5,005 (22.3)	5,780 (25.7)	7,080 (31.5)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	15,250 (67.8)
	4 (102)	6,240 (27.8)	6,835 (30.4)	7,895 (35.1)	9,665 (43.0)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
	5 (127)	8,720 (38.8)	9,555 (42.5)	11,030 (49.1)	13,510 (60.1)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)
	6 (152)	11,465 (51.0)	12,560 (55.9)	14,500 (64.5)	17,760 (79.0)	24,690 (109.8)	27,045 (120.3)	31,230 (138.9)	38,250 (170.1)
3/4	4 (102)	6,240 (27.8)	6,835 (30.4)	7,895 (35.1)	9,665 (43.0)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
	5 (127)	8,720 (38.8)	9,555 (42.5)	11,030 (49.1)	13,510 (60.1)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)
	6-1/4 (159)	12,190 (54.2)	13,350 (59.4)	15,415 (68.6)	18,880 (84.0)	26,250 (116.8)	28,755 (127.9)	33,205 (147.7)	40,665 (180.9)
	7-1/4 (184)	15,225 (67.7)	16,680 (74.2)	19,260 (85.7)	23,590 (104.9)	32,795 (145.9)	35,925 (159.8)	41,485 (184.5)	50,805 (226.0)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Linear interpolation between embedment depths and concrete compressive strengths are not permitted.<sup>3</sup>Compare tabular values to the steel values in Table 4. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.<sup>4</sup>Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>5</sup>Tabular values are for dry and water saturated concrete conditions.<sup>6</sup>Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.<sup>7</sup>Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: For sand-lightweight,  $\lambda_a = 0.51$ . For all-lightweight,  $\lambda_a = 0.45$ .<sup>8</sup>Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

Table 3. Hilti Kwik-X Dual Action Carbon Steel Anchor design strength with concrete / bond failure in cracked concrete<sup>1,2,3,4,5,6,7,8</sup>

Nominal anchor diameter in. (mm)	Effective embedment in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
		$f'_c = 2500$ psi (17.2 MPa) lb (kN)	$f'_c = 3000$ psi (20.7 MPa) lb (kN)	$f'_c = 4000$ psi (27.6 MPa) lb (kN)	$f'_c = 6000$ psi (41.4 MPa) lb (kN)	$f'_c = 2500$ psi (17.2 MPa) lb (kN)	$f'_c = 3000$ psi (20.7 MPa) lb (kN)	$f'_c = 4000$ psi (27.6 MPa) lb (kN)	$f'_c = 6000$ psi (41.4 MPa) lb (kN)
3/8	2-1/2 (64)	2,000 (8.9)	2,050 (9.1)	2,135 (9.5)	2,260 (10.1)	4,310 (19.2)	4,420 (19.7)	4,600 (20.5)	4,870 (21.7)
	3-1/4 (83)	3,235 (14.4)	3,545 (15.8)	4,095 (18.2)	5,015 (22.3)	6,970 (31.0)	7,640 (34.0)	8,820 (39.2)	10,800 (48.0)
	4-1/2 (114)	5,275 (23.5)	5,780 (25.7)	6,670 (29.7)	7,790 (34.7)	11,360 (50.5)	12,445 (55.4)	14,370 (63.9)	16,780 (74.7)
1/2	3 (76)	2,870 (12.8)	3,145 (14.0)	3,630 (16.1)	4,450 (19.8)	6,185 (27.5)	6,775 (30.1)	7,820 (34.8)	9,580 (42.6)
	4-1/4 (108)	4,840 (21.5)	5,305 (23.6)	6,125 (27.2)	7,500 (33.4)	10,425 (46.4)	11,420 (50.8)	13,190 (58.7)	16,150 (71.8)
	5-1/2 (140)	7,125 (31.7)	7,805 (34.7)	9,015 (40.1)	11,040 (49.1)	15,350 (68.3)	16,815 (74.8)	19,415 (86.4)	23,780 (105.8)
5/8	3-1/4 (83)	3,235 (14.4)	3,545 (15.8)	4,095 (18.2)	5,015 (22.3)	6,970 (31.0)	7,640 (34.0)	8,820 (39.2)	10,800 (48.0)
	4 (102)	4,420 (19.7)	4,840 (21.5)	5,590 (24.9)	6,845 (30.4)	9,520 (42.3)	10,430 (46.4)	12,040 (53.6)	14,750 (65.6)
	5 (127)	6,175 (27.5)	6,765 (30.1)	7,815 (34.8)	9,570 (42.6)	13,305 (59.2)	14,575 (64.8)	16,830 (74.9)	20,610 (91.7)
	6 (152)	8,120 (36.1)	8,895 (39.6)	10,270 (45.7)	12,580 (56.0)	17,490 (77.8)	19,160 (85.2)	22,120 (98.4)	27,095 (120.5)
3/4	4 (102)	4,420 (19.7)	4,840 (21.5)	5,590 (24.9)	6,845 (30.4)	9,520 (42.3)	10,430 (46.4)	12,040 (53.6)	14,750 (65.6)
	5 (127)	6,175 (27.5)	6,765 (30.1)	7,815 (34.8)	9,570 (42.6)	13,305 (59.2)	14,575 (64.8)	16,830 (74.9)	20,610 (91.7)
	6-1/4 (159)	8,635 (38.4)	9,455 (42.1)	10,920 (48.6)	13,375 (59.5)	18,595 (82.7)	20,370 (90.6)	23,520 (104.6)	28,805 (128.1)
	7-1/4 (184)	10,785 (48.0)	11,815 (52.6)	13,645 (60.7)	16,710 (74.3)	23,230 (103.3)	25,445 (113.2)	29,385 (130.7)	35,990 (160.1)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Linear interpolation between embedment depths and concrete compressive strengths is not permitted.<sup>3</sup>Compare tabular values to the steel values in Table 4. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.<sup>4</sup>Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>5</sup>Tabular values are for dry and water saturated concrete conditions.<sup>6</sup>Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.<sup>7</sup>Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_s$  as follows: For sand-lightweight,  $\lambda_s = 0.51$ . For all-lightweight,  $\lambda_s = 0.45$ .<sup>8</sup>Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tubular values in tension and shear by  $\alpha_{seis} = 0.75$ . See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.Table 4. Steel design strength for Hilti KH-EZ / KH-EZ CRC anchors<sup>1,2</sup>

Nominal anchor diameter in.	Tensile <sup>3</sup> $\phi N_{sa}$ lb (kN)	Shear <sup>4</sup> $\phi V_{sa}$ lb (kN)	Seismic Shear <sup>5</sup> $\phi V_{sa}$ lb (kN)
3/8	6,720 (29.9)	3,110 (13.8)	1,865 (8.3)
1/2	11,780 (52.4)	5,545 (24.7)	3,330 (14.8)
5/8	15,735 (70.0)	6,735 (30.0)	4,040 (18.0)
3/4	20,810 (92.6)	9,995 (44.5)	6,935 (30.8)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Hilti KH-EZ / KH-EZ CRC anchors are to be considered brittle steel elements.<sup>3</sup>Tensile  $\phi N_{sa} = \phi A_{se,N} f_{utu}$  as noted in ACI 318 Chapter 17.<sup>4</sup>Shear values determined by static shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{utu}$  as noted in ACI 318 Chapter 17.<sup>5</sup>Seismic shear values determined by seismic shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{utu}$  as noted in ACI 318 Chapter 17. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

**Figure 3. Hilti Kwik-X Dual Action SS316 Anchor installation conditions**

Permissible Base Material	Uncracked concrete		Dry concrete	Permissible Drilling Method		Hammer drilling with carbide tipped drill bit
	Cracked concrete		Water-saturated concrete			Hilti TE-CD or TE-YD hollow drill bit (except 3/8" diameter)
						Diamond core drill bit (except 3/8" diameter)

**Table 5. Hilti Kwik-X Dual Action SS316 anchor installation specifications**

Design information	Symbol	Units	Nominal anchor diameter (in.)		
			3/8	1/2	
Drill hole diameter	$d_o$	in.	3/8	1/2	
Minimum fixture hole diameter	$d_f$	in.	1/2	5/8	
Nominal embedment <sup>1</sup>	$h_{nom}$	in. (mm)	2-1/2 – 3 (64 – 76)	3 – 3-1/4 (76 – 83)	3 – 4-1/4 (76 – 108)
KHC Capsule size	-	-	3/8" Small	3/8" Large	1/2" Small
Drilled hole depth <sup>2</sup>	Hole condition 1	$h_1$	in. (mm)	N/A	N/A
	Hole condition 2	$h_1$	in. (mm)	$h_{nom} + 3/8$ ( $h_{nom} + 10$ )	$h_{nom} + 3/8$ ( $h_{nom} + 10$ )
Minimum anchor spacing	$s_{min}$	in. (mm)	3 (76)	3	(76)
Minimum edge distance	$c_{min}$	in. (mm)	1-1/2 (38)	1-3/4 (44)	
Minimum concrete thickness	$h_{min}$	in. (mm)	$h_1 + 1-1/4$ ( $h_1 + 32$ )	$h_1 + 1-1/4$ ( $h_1 + 32$ )	

<sup>1</sup>Nominal embedment ( $h_{nom}$ ) = effective embedment ( $h_{ef}$ ).

<sup>2</sup>See Figure 2 for description of drilled hole conditions.

**Table 6. Steel Design Strength for Hilti KH-EZ SS316 Anchors<sup>1,2,3</sup>**

Anchor Diameter in.	Tensile <sup>4</sup> $\phi N_{sa}$ lb (kN)	Shear <sup>5</sup> $\phi V_{sa}$ lb (kN)	Seismic Shear <sup>6</sup> $\phi V_{sa}$ lb (kN)
3/8	9,820 (43.7)	2,830 (12.6)	2,830 (12.6)
1/2	15,490 (68.9)	3,115 (13.9)	3,115 (13.9)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

<sup>2</sup>Hilti KH-EZ SS316 anchors are to be considered ductile steel elements.

<sup>3</sup>Tensile  $\phi N_{sa} = \phi A_{se,N} f_{uta}$  as noted in ACI 318 Chapter 17.

<sup>4</sup>Shear values determined by static shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$  as noted in ACI 318 Chapter 17.

<sup>5</sup>Seismic shear values determined by seismic shear tests with  $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$  as noted in ACI 318 Chapter 17.

<sup>6</sup>See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Table 7. Hilti Kwik-X Dual Action SS316 anchor design strength with concrete / bond failure in uncracked concrete<sup>1,2,3,4,5,6,7,8</sup>

Nominal anchor diameter in. (mm)	Effective embedment in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
		$f_c = 2500 \text{ psi}$ ( $17.2 \text{ MPa}$ ) lb (kN)	$f_c = 3000 \text{ psi}$ ( $20.7 \text{ MPa}$ ) lb (kN)	$f_c = 4000 \text{ psi}$ ( $27.6 \text{ MPa}$ ) lb (kN)	$f_c = 6000 \text{ psi}$ ( $41.4 \text{ MPa}$ ) lb (kN)	$f_c = 2500 \text{ psi}$ ( $17.2 \text{ MPa}$ ) lb (kN)	$f_c = 3000 \text{ psi}$ ( $20.7 \text{ MPa}$ ) lb (kN)	$f_c = 4000 \text{ psi}$ ( $27.6 \text{ MPa}$ ) lb (kN)	$f_c = 6000 \text{ psi}$ ( $41.4 \text{ MPa}$ ) lb (kN)
3/8	2-1/2 (64)	3,085	3,375	3,900	4,725	6,640	7,275	8,400	10,180
	3-1/4 (83)	4,405	4,720	5,265	6,145	9,490	10,170	11,345	13,235
1/2 <sup>9</sup>	3 (76)	4,055	4,440	5,125	6,280	8,730	9,565	11,040	13,525
	4-1/4 (108)	5,925	6,490	7,490	9,175	12,760	13,975	16,135	19,765

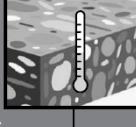
Table 8. Hilti Kwik-X Dual Action SS316 anchor design strength with concrete / bond failure in cracked concrete<sup>1,2,3,4,5,6,7,8,9</sup>

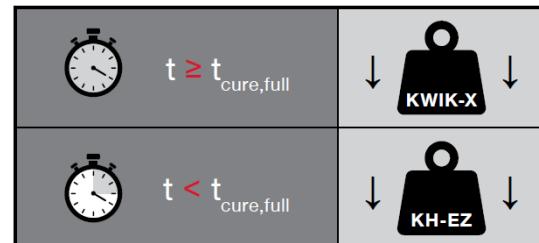
Nominal anchor diameter in. (mm)	Effective embedment in. (mm)	Tension - $\phi N_n$				Shear - $\phi V_n$			
		$f_c = 2500 \text{ psi}$ ( $17.2 \text{ MPa}$ ) lb (kN)	$f_c = 3000 \text{ psi}$ ( $20.7 \text{ MPa}$ ) lb (kN)	$f_c = 4000 \text{ psi}$ ( $27.6 \text{ MPa}$ ) lb (kN)	$f_c = 6000 \text{ psi}$ ( $41.4 \text{ MPa}$ ) lb (kN)	$f_c = 2500 \text{ psi}$ ( $17.2 \text{ MPa}$ ) lb (kN)	$f_c = 3000 \text{ psi}$ ( $20.7 \text{ MPa}$ ) lb (kN)	$f_c = 4000 \text{ psi}$ ( $27.6 \text{ MPa}$ ) lb (kN)	$f_c = 6000 \text{ psi}$ ( $41.4 \text{ MPa}$ ) lb (kN)
3/8	2-1/2 (64)	1,665	1,760	1,925	2,185	3,585	3,795	4,150	4,705
	3-1/4 (83)	3,200	3,385	3,700	4,195	6,890	7,290	7,970	9,035
1/2 <sup>9</sup>	3 (76)	2,870	3,145	3,630	4,450	6,185	6,775	7,820	9,580
	4-1/4 (108)	4,840	5,305	6,125	7,500	10,425	11,420	13,190	16,150

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Linear interpolation between embedment depths and concrete compressive strengths is not permitted.<sup>3</sup>Compare tabular values to the steel values in Table 6. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.<sup>4</sup>Data is for temperature range A: Max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). For temperature range B: Max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C) multiply above values by 0.98. Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>5</sup>Tabular values are for dry and water saturated concrete conditions.<sup>6</sup>Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.<sup>7</sup>Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda$  as follows:<sup>8</sup>For sand-lightweight,  $\lambda_s = 0.51$ . For all-lightweight,  $\lambda_a = 0.45$ .<sup>9</sup>Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tubular values in tension and shear by  $a_{seis} = 0.75$ . See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

The Kwik-X Dual Action Anchor system will provide greater load capacities with greater flexibility. This includes immediate loading in a vast range of temperatures. The amount of load capacity immediately available after installation of the Kwik-X Dual Action Anchor system will vary depending on the concrete temperature at the time of installation. As shown in Figure 3 below, in the very cold spectrum of temperatures the immediate load capacity available will be that of the Hilti KH-EZ / KH-EZ CRC KH-EZ SS316 screw anchor until the full cure time has elapsed. For the load capacity of the Hilti KH-EZ / KH-EZ CRC / KH-EZ SS316 screw anchor please refer to ESR-3027 or Section 3.3.6 or 3.3.7 of PTG Ed. 22.

Figure 4. Cure time and immediate load allowance

	$^{\circ}\text{C}$	$^{\circ}\text{F}$		$^{\circ}\text{C}$	$^{\circ}\text{F}$		$t_{\text{cure,full}}$
-28 ... -10	-18 ... 14	5 ... 40	41 ... 104	24 h			
-10 ... 5	14 ... 41	5 ... 40	41 ... 104	30 min			
5 ... 40	41 ... 104	5 ... 40	41 ... 104	0.5 min			



# Design Data in Concrete per CSA A23.3

## CSA A23.3 Annex D Design

This section contains the Limit State Design tables with un-factored characteristic loads and pre-calculated factored resistance tables based on the published loads in ICC Evaluation Services ESR-5065 and testing per ACI 355.4.

For a detailed explanation of the tables developed in accordance with CSA A23.3 Annex D, refer to Sections 3.1.7 and 3.1.8 of the 2022 PTG Ed. 22. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at [www.hilti.ca](http://www.hilti.ca).

**Table 9. Hilti Kwik-X Dual Action Carbon Steel Anchor design information in hammer drilled and/or core drilled holes in accordance with CSA A23.3 Annex D<sup>1</sup>**

Design Parameter	Symbol	Units	KH-EZ/KH-EZ CRC Anchor diameter (in.)				Ref A23.3	
			3/8	1/2	5/8	3/4		
Nominal anchor diameter	$d_a$	mm	9.5	12.7	15.9	19.1		
Effective minimum embedment <sup>2</sup>	$h_{ef,min}$	mm	64	76	76	83	102	
Effective maximum embedment <sup>2</sup>	$h_{ef,max}$	mm	76	114	140	152	184	
Minimum concrete thickness <sup>2</sup>	$h_{min}$	mm	See Table 1 and Figure 2 of this document					
Critical edge distance	$c_{ac}$	-	See ESR-5065, section 4.1.10					
Minimum edge distance	$c_{min}$	mm	38	44	44	44		
Minimum anchor spacing	$s_{min}$	mm	76	76	102	102		
Coeff. for factored concrete breakout resistance, uncracked concrete	$k_{c,uncr}^3$	-	10				D.6.2.2	
Coeff. for factored concrete breakout resistance, cracked concrete	$k_{c,cr}^3$	-	7				D.6.2.2	
Concrete material resistance factor	$\phi_c$	-	0.65				8.4.2	
Resistance modification factor for tension and shear, concrete failure modes, Condition B4	$R_{conc}$	-	100				D.5.3(c)	
Minimum specified ultimate strength	$f_{uta}$	psi (N/mm <sup>2</sup> )	120,300 (829)	112,540 (776)	90,180 (622)	81,600 (563)		
Effective tensile stress area	$A_{se,N}$	in <sup>2</sup> (mm <sup>2</sup> )	0.086 (55.5)	0.161 (103.9)	0.268 (172.9)	0.392 (252.9)		
Steel embedment material resistance factor for reinforcement	$\phi_s$	-	0.85				8.4.3	
Resistance modification factor for tension, steel failure modes <sup>4</sup>	$R$	-	0.70				D.5.3	
Resistance modification factor for shear, steel failure modes <sup>4</sup>	$R$	-	0.65				D.5.3	
Factored steel resistance intension	$N_{sar}$	lb (kN)	6,150 (27.4)	10,780 (48.0)	14,405 (64.1)	19,050 (84.7)	D.6.1.2	
Effective tensile stress area	$V_{sar}$	lb (kN)	2,865 (12.7)	5,110 (22.7)	6,200 (64.1)	9,205 (40.9)	D.7.1.2	
Effective tensile stress area	$V_{sar,eq}$	lb (kN)	1,720 (7.7)	3,065 (13.6)	3,720 (16.5)	6,385 (28.4)		
Temperature Range <sup>5</sup>	Characteristic bond stress in cracked concrete <sup>6</sup>	$T_{cr}$	psi (MPa)	1,045 (7.2)	2,000 (13.8)	1,900 (13.1)	1,800 (12.4)	D.6.5.2
	Characteristic bond stress in uncracked concrete <sup>6</sup>	$T_{uncr}$	psi (MPa)	2,235 (15.4)	2,125 (14.7)	2,020 (13.9)	1,915 (13.2)	D.6.5.2
Reduction for seismic tension	$\alpha_{N,seis}$	-	1.00					
Permissible installation conditions	Resistance modification factor tension and shear, bond failure dry and water saturated concrete	Anchor category	-	1				D.5.3(c)
		$R_{dry,ws}$	-	1.00				

<sup>1</sup>Design information in this table is taken from ICC-ES ESR-5065 and converted for use with CSA A23.3 Annex D.

<sup>2</sup>See Table 1 and Figure 2 of this document.

<sup>3</sup>For all design cases,  $\psi_{c,N} = 1.0$ . The appropriate coefficient for breakout resistance for cracked concrete ( $k_{c,cr}$ ) or uncracked concrete ( $k_{c,uncr}$ ) must be used.

<sup>4</sup>For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or where pullout or prout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.

<sup>5</sup>Temperature range A: Max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). Temperature range B: Max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>6</sup>Bond strength values corresponding to concrete compressive strength  $f_c = 2,500$  psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^n$  [for SI:  $(f_c / 17.2)^n$ ] where  $n$  is as follows:  $n = 0.38$  and  $n = 0.50$  for 3/8" and 1/2" respectively, in uncracked concrete, hammer drilling with carbide bit;  $n = 0.31$  and  $n = 0.39$  for 3/8" and 1/2" respectively, in cracked concrete, hammer drilling with carbide bit;  $n = 0.50$  for 1/2" in uncracked and cracked concrete, diamond core bit drilling

Table 10. Hilti Kwik-X Dual Action Carbon Steel anchor factored resistance with concrete / bond failure in uncracked concrete<sup>1,2,3,4,5,6,7,8,9</sup>

Nominal anchor diameter in. (mm)	Effective embedment in. (mm)	Tension - Nr				Shear - Vr			
		$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	3,305 (14.7)	3,695 (16.4)	4,050 (18.0)	4,675 (20.8)	6,615 (29.4)	7,395 (32.9)	8,100 (36.0)	9,355 (41.6)
	3-1/4 (83)	4,900 (21.8)	5,480 (24.4)	6,005 (26.7)	6,475 (28.8)	9,805 (43.6)	10,960 (48.8)	12,005 (53.4)	12,950 (57.6)
	4-1/2 (114)	7,910 (35.2)	8,235 (36.6)	8,510 (37.9)	8,965 (39.9)	15,825 (70.4)	16,475 (73.3)	17,025 (75.7)	17,930 (79.7)
1/2	3 (76)	4,345 (19.3)	4,860 (21.6)	5,325 (23.7)	6,145 (27.3)	8,695 (38.7)	9,720 (43.2)	10,650 (47.4)	12,295 (54.7)
	4-1/4 (108)	7,330 (32.6)	8,195 (36.5)	8,975 (39.9)	10,365 (46.1)	14,660 (65.2)	16,390 (72.9)	17,955 (79.9)	20,730 (92.2)
	5-1/2 (140)	10,790 (48.0)	12,065 (53.7)	13,190 (58.7)	13,890 (61.8)	21,580 (96.0)	24,130 (107.3)	26,375 (117.3)	27,780 (123.6)
5/8	3-1/4 (83)	4,900 (21.8)	5,480 (24.4)	6,005 (26.7)	6,930 (30.8)	9,805 (43.6)	10,960 (48.8)	12,005 (53.4)	13,865 (61.7)
	4 (102)	6,690 (29.8)	7,480 (33.3)	8,195 (36.5)	9,465 (42.1)	13,385 (59.5)	14,965 (66.6)	16,395 (72.9)	18,930 (84.2)
	5 (127)	9,355 (41.6)	10,455 (46.5)	11,455 (51.0)	13,225 (58.8)	18,705 (83.2)	20,915 (93.0)	22,910 (101.9)	26,455 (117.7)
	6 (152)	12,295 (54.7)	13,745 (61.1)	15,060 (67.0)	17,385 (77.3)	24,590 (109.4)	27,490 (122.3)	30,115 (134.0)	34,775 (154.7)
3/4	4 (102)	6,690 (29.8)	7,480 (33.3)	8,195 (36.5)	9,465 (42.1)	13,385 (59.5)	14,965 (66.6)	16,395 (72.9)	18,930 (84.2)
	5 (127)	9,355 (41.6)	10,455 (46.5)	11,455 (51.0)	13,225 (58.8)	18,705 (83.2)	20,915 (93.0)	22,910 (101.9)	26,455 (117.7)
	6-1/4 (159)	13,070 (58.1)	14,615 (65.0)	16,010 (71.2)	18,485 (82.2)	26,140 (116.3)	29,230 (130.0)	32,020 (142.4)	36,970 (164.5)
	7-1/4 (184)	16,330 (72.6)	18,260 (81.2)	20,000 (89.0)	23,095 (102.7)	32,660 (145.3)	36,515 (162.4)	40,000 (177.9)	46,190 (205.5)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Linear interpolation between embedment depths and concrete compressive strengths is not permitted.<sup>3</sup>Compare tabular values to the steel values in Table 12. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.<sup>4</sup>Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C).<sup>5</sup>Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>6</sup>Tabular values are for dry and water saturated concrete conditions.<sup>7</sup>Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.<sup>8</sup>Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: For sand-lightweight,  $\lambda_a = 0.51$ . For all-lightweight,  $\lambda_a = 0.45$ .<sup>9</sup>Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

Table 11. Hilti Kwik-X Dual Action Carbon Steel anchor factored resistance with concrete / bond failure in cracked concrete<sup>1,2,3,4,5,6,7,8</sup>

Nominal anchor diameter in. (mm)	Effective embedment in. (mm)	Tension - $N_r$				Shear - $V_r$			
		$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	2,045 (9.1)	2,110 (9.4)	2,160 (9.6)	2,250 (10.0)	4,085 (18.2)	4,215 (18.8)	4,325 (19.2)	4,505 (20.0)
	3-1/4 (83)	3,430 (15.3)	3,835 (17.1)	4,200 (18.7)	4,850 (21.6)	6,860 (30.5)	7,670 (34.1)	8,405 (37.4)	9,705 (43.2)
	4-1/2 (114)	5,590 (24.9)	6,250 (27.8)	6,845 (30.5)	7,755 (34.5)	11,180 (49.7)	12,500 (55.6)	13,695 (60.9)	15,510 (69.0)
1/2	3 (76)	3,045 (13.5)	3,400 (15.1)	3,725 (16.6)	4,305 (19.1)	6,085 (27.1)	6,805 (30.3)	7,455 (33.2)	8,605 (38.3)
	4-1/4 (108)	5,130 (22.8)	5,735 (25.5)	6,285 (28.0)	7,255 (32.3)	10,260 (45.6)	11,475 (51.0)	12,570 (55.9)	14,510 (64.6)
	5-1/2 (140)	7,555 (33.6)	8,445 (37.6)	9,250 (41.1)	10,680 (47.5)	15,105 (67.2)	16,890 (75.1)	18,500 (82.3)	21,365 (95.0)
5/8	3-1/4 (83)	3,430 (15.3)	3,835 (17.1)	4,200 (18.7)	4,850 (21.6)	6,860 (30.5)	7,670 (34.1)	8,405 (37.4)	9,705 (43.2)
	4 (102)	4,685 (20.8)	5,240 (23.3)	5,740 (25.5)	6,625 (29.5)	9,370 (41.7)	10,475 (46.6)	11,475 (51.0)	13,250 (58.9)
	5 (127)	6,545 (29.1)	7,320 (32.6)	8,020 (35.7)	9,260 (41.2)	13,095 (58.2)	14,640 (65.1)	16,035 (71.3)	18,520 (82.4)
	6 (152)	8,605 (38.3)	9,620 (42.8)	10,540 (46.9)	12,170 (54.1)	17,215 (76.6)	19,245 (85.6)	21,080 (93.8)	24,340 (108.3)
3/4	4 (102)	4,685 (20.8)	5,240 (23.3)	5,740 (25.5)	6,625 (29.5)	9,370 (41.7)	10,475 (46.6)	11,475 (51.0)	13,250 (58.9)
	5 (127)	6,545 (29.1)	7,320 (32.6)	8,020 (35.7)	9,260 (41.2)	13,095 (58.2)	14,640 (65.1)	16,035 (71.3)	18,520 (82.4)
	6-1/4 (159)	9,150 (40.7)	10,230 (45.5)	11,205 (49.8)	12,940 (57.6)	18,300 (81.4)	20,460 (91.0)	22,410 (99.7)	25,880 (115.1)
	7-1/4 (184)	11,430 (50.8)	12,780 (56.9)	14,000 (62.3)	16,165 (71.9)	22,865 (101.7)	25,560 (113.7)	28,000 (124.6)	32,335 (143.8)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Linear interpolation between embedment depths and concrete compressive strengths is not permitted.<sup>3</sup>Compare tabular values to the steel values in Table 12. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.<sup>4</sup>Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>5</sup>Tabular values are for dry and water saturated concrete conditions.<sup>6</sup>Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.<sup>7</sup>Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: For sand-lightweight,  $\lambda_a = 0.51$ . For all-lightweight,  $\lambda_a = 0.45$ .<sup>8</sup>Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tubular values in tension and shear by  $a_{seis} = 0.75$ . See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.Table 12. Steel resistance for Hilti KH-EZ / KH-EZ CRC carbon steel screw anchor<sup>1,2</sup>

Nominal anchor diameter in.	Tensile <sup>3</sup> $N_{sar}$ lb (kN)	Shear <sup>4</sup> $V_{sar}$ lb (kN)	Seismic Shear <sup>5</sup> $V_{sar,eq}$ lb (kN)
3/8	6,150 (27.4)	2,865 (12.7)	1,720 (7.7)
1/2	10,780 (48.0)	5,110 (22.7)	3,065 (13.6)
5/8	14,405 (64.1)	6,200 (27.6)	3,720 (16.5)
3/4	19,050 (84.7)	9,205 (40.9)	6,385 (28.4)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Hilti KH-EZ / KH-EZ CRC carbon steel screw anchors are to be considered brittle steel elements.<sup>3</sup>Tensile  $N_{sar} = A_{se,N} \phi f_{utu} R$  as noted in CSA A23.3 Annex D.<sup>4</sup>Shear determined by static shear tests with  $V_{sar} < 0.6 A_{se,V} \phi f_{utu} R$  as noted in CSA A23.3 Annex D.<sup>5</sup>Seismic shear values determined by seismic shear tests with  $V_{sar,eq} \leq 0.60 A_{se,V} \phi f_{utu} R$  as noted in CSA A23.3 Annex D. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Table 13. Hilti Kwik-X Dual Action SS316 anchor design information in hammer drilled and/or core drilled holes in accordance with CSA A23.3 Annex D<sup>1</sup>

Design parameter	Symbol	Units	Nominal anchor diameter (in.)		Ref A23.3			
			3/8	1/2				
Nominal anchor diameter	$d_a$	mm	9.5	12.7				
Effective minimum embedment <sup>2</sup>	$h_{ef,min}$	mm	64	76	76			
Effective maximum embedment <sup>2</sup>	$h_{ef,max}$	mm	76	83	108			
Min. concrete thickness <sup>2</sup>	$h_{min}$	mm	See Table 1 and Figure 2 of this document					
Critical edge distance	$c_{ac}$	-	See ESR-5065, section 4.1.10					
Minimum edge distance	$c_{min}$	mm	38	45				
Minimum anchor spacing	$s_{min}$	mm	76	76				
Coeff. for factored conc. breakout resistance, uncracked concrete	$k_{c,uncr}^3$	-	10.0		D.6.2.2			
Coeff. for factored conc. breakout resistance, cracked concrete	$k_{c,cr}^3$	-	7.0		D.6.2.2			
Concrete material resistance factor	$\phi_c$	-	0.65		8.4.2			
Resistance modification factor for tension and shear, concrete failure modes, Condition B <sup>4</sup>	$R_{conc}$	-	1.00		D.5.3 (c)			
Minimum specified ultimate strength	$f_{uta}$	psi (N/mm <sup>2</sup> )	139,300 (961)	120,100 (828)				
Effective tensile stress area	$A_{se,N}$	in <sup>2</sup> (mm <sup>2</sup> )	0.094 (60.8)	0.172 (111.2)				
Steel embedment material resistance factor for reinforcement.	$\phi_s$	-	0.85		8.4.3			
Resistance modification factor for tension, steel failure modes <sup>4</sup>	$R$	-	0.80		D.5.3			
Resistance modification factor for shear, steel failure mode <sup>4</sup>	$R$	-	0.75		D.5.3			
Factored steel resistance in tension	$N_{sar}$	lb (kN)	8,905 (39.6)	14,045 (62.5)	D.6.1.2			
Effective tensile stress area	$V_{sar}$	lb (kN)	2,775 (12.3)	3,055 (13.6)	D.7.1.2			
Effective tensile stress area	$V_{sar,eq}$	lb (kN)	2,775 (12.3)	3,055 (13.6)				
Carbide Bit								
Temp. range A <sup>5</sup>	Characteristic bond stress in cracked concrete <sup>6</sup>	$T_{cr}$	psi (MPa)	870 (6.0)	1,285 (8.9)	1,240 (8.6)	D.6.5.2	
	Characteristic bond stress in uncracked concrete <sup>6</sup>	$T_{uncr}$	psi (MPa)	1,770 (12.2)		1,365 (9.4)	D.6.5.2	
Temp. range B <sup>5</sup>	Characteristic bond stress in cracked concrete <sup>6</sup>	$T_{cr}$	psi (MPa)	850 (5.9)	1,255 (8.7)	1,215 (8.4)	D.6.5.2	
	Characteristic bond stress in uncracked concrete <sup>6</sup>	$T_{uncr}$	psi (MPa)	1,730 (11.9)		1,330 (9.2)	D.6.5.2	
Reduction for seismic tension	$a_{N,seis}$	-	1.00					
Diamond Core Drill Bit								
Temp. range A <sup>5</sup>	Characteristic bond stress in cracked concrete <sup>6</sup>	$T_{cr}$	psi (MPa)	N/A		1,005 (6.9)	D.6.5.2	
	Characteristic bond stress in uncracked concrete <sup>6</sup>	$T_{uncr}$	psi (MPa)	N/A		1,295 (8.9)	D.6.5.2	
Temp. range B <sup>5</sup>	Characteristic bond stress in cracked concrete <sup>6</sup>	$T_{cr}$	psi (MPa)	N/A		980 (6.8)	D.6.5.2	
	Characteristic bond stress in uncracked concrete <sup>6</sup>	$T_{uncr}$	psi (MPa)	N/A		1,265 (8.7)	D.6.5.2	
Reduction for seismic tension	$a_{N,seis}$	-	1.00					
Carbide Bit or Diamond Core Drill Bit								
Permissible installation conditions	Resistance modification factor tension & shear, bond failure dry and water saturated concrete	Anchor category	-	1		D.5.3 (c)		
		$R_{dry,ws}$	-	1.00				

<sup>1</sup>Design information in this table is taken from ICC-ES ESR-5065 and converted for use with CSA A23.3 Annex D.<sup>2</sup>See Table 1 and Figure 2 of this document.<sup>3</sup>For all design cases,  $\psi_{c,N} = 1.0$ . The appropriate coefficient for breakout resistance for cracked concrete ( $k_{c,cr}$ ) or uncracked concrete ( $k_{c,uncr}$ ) must be used.<sup>4</sup>For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or where pullout or ptyout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.<sup>5</sup>Temperature range A: Max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). Temperature range B: Max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>6</sup>Bond strength values corresponding to concrete compressive strength  $f_c = 2,500$  psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^n$  [for SI:  $(f_c/17.2)^n$ ] where  $n$  is as follows:  $n = 0.38$  and  $n = 0.50$  for 3/8" and 1/2" respectively, in uncracked concrete, hammer drilling with carbide bit;  $n = 0.31$  and  $n = 0.39$  for 3/8" and 1/2" respectively, in cracked concrete, hammer drilling with carbide bit;  $n = 0.50$  for 1/2" in uncracked and cracked concrete, diamond core bit drilling

Table 14. Hilti Kwik-X SS316 Dual Action anchor factored resistance with concrete / bond failure in uncracked concrete<sup>1,2,3,4,5,6,7,8</sup>

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - $N_r$				Shear - $V_r$			
		$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	3,305 (14.7)	3,695 (16.4)	4,050 (18.0)	4,665 (20.8)	3,305 (14.7)	3,695 (16.4)	4,050 (18.0)	4,665 (20.8)
	3-1/4 (83)	4,660 (20.7)	5,075 (22.6)	5,440 (24.2)	6,065 (27.0)	9,325 (41.5)	10,150 (45.1)	10,875 (48.4)	12,135 (54.0)
1/2 <sup>9</sup>	3 (76)	4,345 (19.3)	4,860 (21.6)	5,325 (23.7)	6,145 (27.3)	8,695 (38.7)	9,720 (43.2)	10,650 (47.4)	12,295 (54.7)
	4-1/4 (108)	6,380 (28.4)	7,135 (31.7)	7,815 (34.8)	9,025 (40.1)	12,760 (56.8)	14,270 (63.5)	15,630 (69.5)	18,050 (80.3)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Linear interpolation between embedment depths and concrete compressive strengths is not permitted.<sup>3</sup>Compare tabular values to the steel values in Table 16. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.<sup>4</sup>Data is for max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.<sup>5</sup>Tabular values are for dry and water saturated concrete conditions.<sup>6</sup>Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.<sup>7</sup>Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by  $\lambda_a$  as follows: For sand-lightweight,  $\lambda_a = 0.51$ . For all-lightweight,  $\lambda_a = 0.45$ .<sup>8</sup>Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tubular values in tension and shear by  $\alpha_{seis} = 0.75$ . See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.<sup>9</sup>Tabular values are for holes drilled in concrete with carbide tipped hammer drill bit. For diamond core drilling with 1/2" diameter anchors only, multiply uncracked concrete tabular values by 0.95 and cracked concrete tabular values by 0.90.Table 15. Hilti Kwik-X SS316 Dual Action anchor factored resistance with concrete / bond failure in cracked concrete<sup>1, 2, 3, 4, 5, 6, 7, 8</sup>

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - $N_r$				Shear - $V_r$			
		$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	1,745 (7.8)	1,870 (8.3)	1,980 (8.8)	2,165 (9.6)	1,745 (7.8)	1,870 (8.3)	1,980 (8.8)	2,165 (9.6)
	3-1/4 (83)	3,350 (14.9)	3,590 (16.0)	3,800 (16.9)	4,150 (18.5)	6,700 (29.8)	7,180 (31.9)	7,595 (33.8)	8,305 (36.9)
1/2 9	3 (76)	3,045 (13.5)	3,400 (15.1)	3,725 (16.6)	4,305 (19.1)	6,085 (27.1)	6,805 (30.3)	7,455 (33.2)	8,605 (38.3)
	4-1/4 (108)	5,130 (22.82)	5,735 (25.52)	6,285 (27.95)	7,255 (32.28)	10,260 (45.64)	11,475 (51.03)	12,570 (55.90)	14,510 (64.55)

Table 16. Steel resistance for Hilti Kwik-X SS316 screw anchor<sup>1,2</sup>

Nominal anchor diameter in.	Tensile <sup>3</sup> $N_{sar}$ lb (kN)	Shear <sup>4</sup> $V_{sar}$ lb (kN)	Seismic Shear <sup>5</sup> $V_{sar,eq}$ lb (kN)
3/8	7,855 (34.9)	2,450 (10.9)	2,450 (10.9)
1/2	14,045 (62.5)	3,055 (13.6)	3,055 (13.6)

<sup>1</sup>See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.<sup>2</sup>Hilti KH-EZ carbon steel screw anchors are to be considered brittle steel elements.<sup>3</sup>Tensile  $N_{sar} = A_{se,N} \phi s f_{ult} R$  as noted in CSA A23.3 Annex D.<sup>4</sup>Shear determined by static shear tests with  $V_{sar} < 0.6 A_{se,v} \phi s f_{ult} R$  as noted in CSA A23.3 Annex D.<sup>5</sup>Seismic shear values determined by seismic shear tests with  $V_{sar,eq} < 0.60 A_{se,v} \phi s f_{ult} R$  as noted in CSA A23.3 Annex D. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

## Product Portfolio



Hilti KHC Kwik-X Capsule



Hilti KH-EZ Screw Anchor



Hilti KH-EZ CRC Screw Anchor



Hilti KH-EZ SS316 Screw Anchor

### Kwik-X Dual Action Anchor

Description	Hole diameter in.	Minimum Embedment	Maximum Embedment	Qty / Box
KHC Kwik-X Capsule 3/8" SMALL	3/8"	2-1/2	3	50
KHC Kwik-X Capsule 3/8" LARGE	3/8"	3	4-1/2	50
KHC Kwik-X Capsule 1/2" SMALL	1/2"	3	4-1/4	25
KHC Kwik-X Capsule 1/2" LARGE	1/2"	4-1/4	5-1/2	25
KHC Kwik-X Capsule 5/8" SMALL	5/8"	3-1/4	4-1/2	24
KHC Kwik-X Capsule 5/8" LARGE	5/8"	4-1/2	6	24
KHC Kwik-X Capsule 3/4" SMALL	3/4"	4	4-1/2	24
KHC Kwik-X Capsule 3/4" LARGE	3/4"	4-1/2	7-1/4	24

### KH-EZ Screw Anchor

Description	Hole diameter in.	Minimum Embedment	Maximum Embedment	Qty / Box
KH-EZ 3/8"x3"	3/8"	2-1/2	3	50
KH-EZ 3/8"x3 1/2"	3/8"	2-1/2	3-1/2	50
KH-EZ 3/8"x4"	3/8"	2 -2	4	50
KH-EZ 3/8"x5"	3/8"	2-1/2	5	30
KH-EZ 1/2"x3 1/2"	1/2"	3	3-1/4	25
KH-EZ 1/2"x4"	1/2"	3	4	25
KH-EZ 1/2"x4 1/2"	1/2"	3	4 1/2	25
KH-EZ 1/2"x5"	1/2"	3	5	25
KH-EZ 1/2"x6"	1/2"	3	6	25
KH-EZ 5/8"x3 1/2"	1/2"	3	3-1/2	15
KH-EZ 5/8"x4"	5/8"	3-1/4	4	15
KH-EZ 5/8"x5 1/2"	5/8"	3-1/4	5-1/2	15
KH-EZ 5/8"x6 1/2"	5/8"	3-1/4	6-1/2	15
KH-EZ 5/8"x8"	5/8"	3-1/4	8	15
KH-EZ 3/4"x4 1/2"	3/4"	4	4-1/2	10
KH-EZ 3/4"x5 1/2"	3/4"	4	5-1/2	10
KH-EZ 3/4"x7"	3/4"	4	7	10
KH-EZ 3/4"x8"	3/4"	4	8	10
KH-EZ 3/4"x9"	3/4"	4	9	10

### KH-EZ CRC Screw Anchor

Description	Hole diameter in.	Minimum Embedment	Maximum Embedment	Qty / Box
KH-EZ CRC 3/8"x3"	3/8"	2-1/2	3	50
KH-EZ CRC 3/8"x4"	3/8"	2-1/2	4	50
KH-EZ CRC 3/8"x5"	3/8"	2-1/2	5	30
KH-EZ CRC 1/2"x4"	1/2"	3	4	25
KH-EZ CRC 1/2"x5"	1/2"	3	5	25
KH-EZ CRC 1/2"x6"	1/2"	3	6	25
KH-EZ CRC 5/8"x5 1/2"	5/8"	3-1/4	5-1/2	15
KH-EZ CRC 5/8"x6 1/2"	5/8"	3-1/4	6-1/2	15
KH-EZ CRC 5/8"x8"	5/8"	3-1/4	8	15
KH-EZ CRC 3/4"x5 1/2"	3/4"	4	5-1/2	10
KH-EZ CRC 3/4"x7"	3/4"	4	7	10
KH-EZ CRC 3/4"x9"	3/4"	4	9	10

## KH-EZ SS316 Screw Anchor

Description	Hole Diameter	Minimum Embedment	Maximum Embedment	Qty / Box
KH-EZ SS316 3/8"x3"	3/8"	2 1/2	3	25
KH-EZ SS316 3/8"x4"	3/8"	2 1/2	4	25
KH-EZ SS316 3/8"x5"	3/8"	2 1/2	5	25
KH-EZ SS316 1/2"x4"	1/2"	3	4	12
KH-EZ SS316 1/2"x5"	1/2"	3	5	12

**In the US:**

Hilti, Inc.  
7250 Dallas Parkway, Suite 1000  
Plano, TX 75024

Customer Service: 1-800-879-8000  
en español: 1-800-879-5000  
Fax: 1-800-879-7000

Hilti is an equal opportunity employer.  
Hilti is a registered trademark of Hilti Corp.  
©Copyright 2025 by Hilti, Inc.

**In Canada:**

Hilti (Canada) Corporation  
2201 Bristol Circle  
Oakville ON | L6H 0J8  
Canada

Customer Service: 1-800-363-4458  
Fax: 1-800-363-4459



The data contained in this literature was current as of the date of publication. Updates and changes may be made based on later testing. If verification is needed that the data is still current, please contact the Hilti Technical Support Specialists at 1-800-879-8000. All published load values contained in this literature represent the results of testing by Hilti or test organizations. Local base materials were used. Because of variations in materials, on-site testing is necessary to determine performance at any specific site. Printed in the United States.