



TECHNICAL SUPPLEMENT

Kwik-X Dual Action Anchor

January, 2026



Kwik-X Dual Action Anchor System

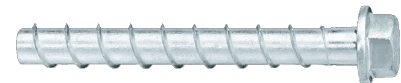
KWIK-X Dual Action Anchor consisting of KHC Capsule and KH-EZ / KH-EZ CRC / KH-EZ SS316 screw anchors

Features and Benefits

- Combines the high performance of adhesive anchors with the speed and simplicity of screw anchors
- Evaluated by ICC Evaluation Services for cracked concrete and seismic service
- No hole cleaning required for carbon steel anchors – helping save time and eliminating the need for accessories like air compressors and brushes
- OSHA Table 1926.1153 Table 1 compliant installation when installed with Hilti vacuum and DRS system or Hilti SafeSet™ hollow drill bit technology
- Suitable for real jobsite conditions – including water saturated concrete and low installation temperatures
- Screw is fully removable and reusable in the same borehole (one time remove and reuse only, not covered in ESR-5065)
- Immediate loading possible



Hilti KHC Kwik-X capsule



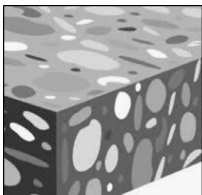
Hilti KH-EZ screw anchor



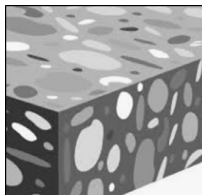
Hilti KH-EZ CRC screw anchor (Mechanically Galvanized)



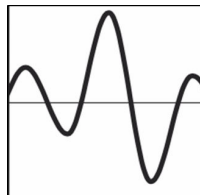
Hilti KH-EZ SS316 screw anchor



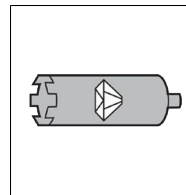
Uncracked concrete



Cracked concrete



Seismic design categories A-F



Diamond core drilling permitted (except for 3/8" Kwik-X SS316 anchors)



Hollow drill bit



PROFIS Engineering Design Software

Approvals / Listings

ICC-ES (International Code Council)	ESR-5065 in concrete per ACI 318 Ch. 17 / ACI 355.4 / ICC-ES AC308
NSF/ANSI Std 61	Certification for use in potable water
City of Los Angeles	LABC Supplement (within ESR-5065)
Florida Building Code	FBC Supplement (within ESR-5065) w/ HVHZ
U.S. Green Building Council	LEED® Credit 4.1-Low Emitting Materials



Design Data in Concrete per ACI 318

ACI 318 Chapter 17 Design

The load tables in this section were developed using the Strength Design parameters and variables of ESR-5065 and the equations within ACI 318 Chapter 17. For more information on ACI 318 Ch. 17 design and the Hilti Simplified Design Tables, refer to sections 3.1.6 and 3.1.8 of the North American Product Technical Guide, Volume 2: Anchor Fastening Technical Guide, Edition 22 (PTG Ed. 22). Data tables from ESR-5065 are not contained in this section but can be found at www.icc-es.org or at www.hilti.com.

Figure 1. Hilti Kwik-X Dual Action Carbon Steel Anchor Installation Conditions


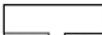





Permissible Base Material		Uncracked concrete		Dry concrete	Permissible Drilling Method		Hammer drilling with carbide tipped drill bit
		Cracked concrete		Water-saturated concrete			Hilti TE-CD or TE-YD hollow drill bit (except 3/8" diameter)
							Diamond core drill bit

Table 1. Hilti Kwik-X Dual Action with KH-EZ and KH-EZ CRC Screw Anchors Installation Specifications

Design information		Symbol	Units	KH-EZ / KH-EZ CRC anchor diameter (in.)							
				3/8		1/2		5/8		3/4	
Drill hole diameter		d_o	in.	3/8		1/2		5/8		3/4	
Minimum fixture hole diameter		d_f	in.	1/2		5/8		3/4		7/8	
Nominal embedment ¹		h_{nom}	in. (mm)	2-1/2 - 3 (64 - 76)	3 - 4-1/2 (76 - 114)	3 - 4-1/4 (76 - 108)	4-1/4 - 5-1/2 (108 - 140)	3-1/4 - 4-1/2 (83 - 114)	4-1/2 - 6 (114 - 152)	4 - 4-1/2 (102 - 114)	4-1/2 - 7-1/4 (114 - 184)
KHC capsule size		-	-	3/8" Small	3/8" Large	1/2" Small	1/2" Large	5/8" Small	5/8" Large	3/4" Small	3/4" Large
Drilled hole depth ²	Hole condition 1	h_1	in. (mm)	$h_{nom} + 5/8$ ($h_{nom} + 16$)		$h_{nom} + 3/4$ ($h_{nom} + 19$)		$h_{nom} + 1-5/8$ ($h_{nom} + 41$)		$h_{nom} + 1-7/8$ ($h_{nom} + 48$)	
	Hole condition 2	h_2	in. (mm)	$h_{nom} + 3/8$ ($h_{nom} + 10$)		$h_{nom} + 3/8$ ($h_{nom} + 10$)		$h_{nom} + 3/8$ ($h_{nom} + 10$)		$h_{nom} + 3/8$ ($h_{nom} + 10$)	
Minimum anchor spacing		s_{min}	in. (mm)	3 (76)		3 (76)		4 (102)		4 (102)	
Minimum edge distance		c_{min}	in. (mm)	1-1/2 (38)		1-3/4 (44)		1-3/4 (44)		1-3/4 (44)	
Minimum concrete thickness		h_{min}	in. (mm)	$h_1 + 1-1/4$ ($h_1 + 32$)		$h_1 + 1-1/4$ ($h_1 + 32$)		$h_1 + 1-1/4$ ($h_1 + 32$)		$h_1 + 1-1/2$ ($h_1 + 38$)	

¹Nominal embedment (h_{nom}) = effective embedment (h_{ef}).

²See Figure 2 for description of drilled hole conditions.

Figure 2. Drilled hole conditions for Kwik-X Dual Action Anchors

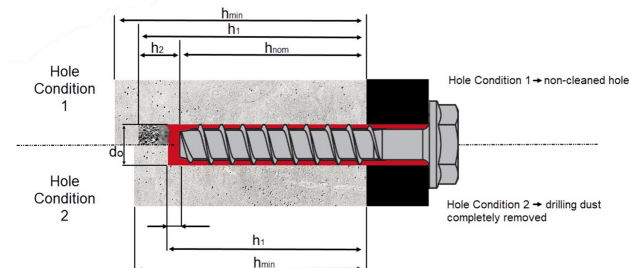


Table 2. Hilti Kwik-X Dual Action Anchor Carbon Steel design strength with concrete / bond failure in uncracked concrete^{1,2,3,4,5,6,7,8}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - ϕN_n				Shear - ϕV_n			
		$f'_c = 2500$ psi (17.2 MPa) lb (kN)	$f'_c = 3000$ psi (20.7 MPa) lb (kN)	$f'_c = 4000$ psi (27.6 MPa) lb (kN)	$f'_c = 6000$ psi (41.4 MPa) lb (kN)	$f'_c = 2500$ psi (17.2 MPa) lb (kN)	$f'_c = 3000$ psi (20.7 MPa) lb (kN)	$f'_c = 4000$ psi (27.6 MPa) lb (kN)	$f'_c = 6000$ psi (41.4 MPa) lb (kN)
3/8	2-1/2 (64)	3,085 (13.7)	3,375 (15.0)	3,900 (17.3)	4,775 (21.2)	6,640 (29.5)	7,275 (32.4)	8,400 (37.4)	10,290 (45.8)
	3-1/4 (83)	4,570 (20.3)	5,005 (22.3)	5,780 (25.7)	6,510 (29.0)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	14,025 (62.4)
	4-1/2 (114)	7,445 (33.1)	7,960 (35.4)	8,380 (37.3)	9,015 (40.1)	16,035 (71.3)	17,140 (76.2)	18,055 (80.3)	19,420 (86.3)
1/2	3 (76)	4,055 (18.0)	4,440 (19.8)	5,125 (22.8)	6,280 (27.9)	8,730 (38.8)	9,565 (42.5)	11,040 (49.1)	13,525 (60.2)
	4-1/4 (108)	6,835 (30.4)	7,485 (33.3)	8,645 (38.5)	10,585 (47.1)	14,720 (65.5)	16,125 (71.7)	18,620 (82.8)	22,805 (101.4)
	5-1/2 (140)	10,060 (44.7)	11,020 (49.0)	12,725 (56.6)	13,970 (62.2)	21,670 (96.4)	23,740 (105.6)	27,410 (121.9)	30,090 (134.0)
5/8	3-1/4 (83)	4,570 (20.3)	5,005 (22.3)	5,780 (25.7)	7,080 (31.5)	9,845 (43.8)	10,785 (48.0)	12,450 (55.4)	15,250 (67.8)
	4 (102)	6,240 (27.8)	6,835 (30.4)	7,895 (35.1)	9,665 (43.0)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
	5 (127)	8,720 (38.8)	9,555 (42.5)	11,030 (49.1)	13,510 (60.1)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)
	6 (152)	11,465 (51.0)	12,560 (55.9)	14,500 (64.5)	17,760 (79.0)	24,690 (109.8)	27,045 (120.3)	31,230 (138.9)	38,250 (170.1)
3/4	4 (102)	6,240 (27.8)	6,835 (30.4)	7,895 (35.1)	9,665 (43.0)	13,440 (59.8)	14,725 (65.5)	17,000 (75.6)	20,820 (92.6)
	5 (127)	8,720 (38.8)	9,555 (42.5)	11,030 (49.1)	13,510 (60.1)	18,785 (83.6)	20,575 (91.5)	23,760 (105.7)	29,100 (129.4)
	6-1/4 (159)	12,190 (54.2)	13,350 (59.4)	15,415 (68.6)	18,880 (84.0)	26,250 (116.8)	28,755 (127.9)	33,205 (147.7)	40,665 (180.9)
	7-1/4 (184)	15,225 (67.7)	16,680 (74.2)	19,260 (85.7)	23,590 (104.9)	32,795 (145.9)	35,925 (159.8)	41,485 (184.5)	50,805 (226.0)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Linear interpolation between embedment depths and concrete compressive strengths are not permitted.

³Compare tabular values to the steel values in Table 4. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.

⁴Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁵Tabular values are for dry and water saturated concrete conditions.

⁶Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.

⁷Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: For sand-lightweight, $\lambda_a = 0.51$. For all-lightweight, $\lambda_a = 0.45$.

⁸Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

Table 3. Hilti Kwik-X Dual Action Carbon Steel Anchor design strength with concrete / bond failure in cracked concrete^{1,2,3,4,5,6,7,8}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - ϕN_n				Shear - ϕV_n			
		$f'_c = 2500 \text{ psi}$ (17.2 MPa) lb (kN)	$f'_c = 3000 \text{ psi}$ (20.7 MPa) lb (kN)	$f'_c = 4000 \text{ psi}$ (27.6 MPa) lb (kN)	$f'_c = 6000 \text{ psi}$ (41.4 MPa) lb (kN)	$f'_c = 2500 \text{ psi}$ (17.2 MPa) lb (kN)	$f'_c = 3000 \text{ psi}$ (20.7 MPa) lb (kN)	$f'_c = 4000 \text{ psi}$ (27.6 MPa) lb (kN)	$f'_c = 6000 \text{ psi}$ (41.4 MPa) lb (kN)
3/8	2-1/2 (64)	2,000 (8.9)	2,050 (9.1)	2,135 (9.5)	2,260 (10.1)	4,310 (19.2)	4,420 (19.7)	4,600 (20.5)	4,870 (21.7)
	3-1/4 (83)	3,235 (14.4)	3,545 (15.8)	4,095 (18.2)	5,015 (22.3)	6,970 (31.0)	7,640 (34.0)	8,820 (39.2)	10,800 (48.0)
	4-1/2 (114)	5,275 (23.5)	5,780 (25.7)	6,670 (29.7)	7,790 (34.7)	11,360 (50.5)	12,445 (55.4)	14,370 (63.9)	16,780 (74.7)
1/2	3 (76)	2,870 (12.8)	3,145 (14.0)	3,630 (16.1)	4,450 (19.8)	6,185 (27.5)	6,775 (30.1)	7,820 (34.8)	9,580 (42.6)
	4-1/4 (108)	4,840 (21.5)	5,305 (23.6)	6,125 (27.2)	7,500 (33.4)	10,425 (46.4)	11,420 (50.8)	13,190 (58.7)	16,150 (71.8)
	5-1/2 (140)	7,125 (31.7)	7,805 (34.7)	9,015 (40.1)	11,040 (49.1)	15,350 (68.3)	16,815 (74.8)	19,415 (86.4)	23,780 (105.8)
5/8	3-1/4 (83)	3,235 (14.4)	3,545 (15.8)	4,095 (18.2)	5,015 (22.3)	6,970 (31.0)	7,640 (34.0)	8,820 (39.2)	10,800 (48.0)
	4 (102)	4,420 (19.7)	4,840 (21.5)	5,590 (24.9)	6,845 (30.4)	9,520 (42.3)	10,430 (46.4)	12,040 (53.6)	14,750 (65.6)
	5 (127)	6,175 (27.5)	6,765 (30.1)	7,815 (34.8)	9,570 (42.6)	13,305 (59.2)	14,575 (64.8)	16,830 (74.9)	20,610 (91.7)
	6 (152)	8,120 (36.1)	8,895 (39.6)	10,270 (45.7)	12,580 (56.0)	17,490 (77.8)	19,160 (85.2)	22,120 (98.4)	27,095 (120.5)
3/4	4 (102)	4,420 (19.7)	4,840 (21.5)	5,590 (24.9)	6,845 (30.4)	9,520 (42.3)	10,430 (46.4)	12,040 (53.6)	14,750 (65.6)
	5 (127)	6,175 (27.5)	6,765 (30.1)	7,815 (34.8)	9,570 (42.6)	13,305 (59.2)	14,575 (64.8)	16,830 (74.9)	20,610 (91.7)
	6-1/4 (159)	8,635 (38.4)	9,455 (42.1)	10,920 (48.6)	13,375 (59.5)	18,595 (82.7)	20,370 (90.6)	23,520 (104.6)	28,805 (128.1)
	7-1/4 (184)	10,785 (48.0)	11,815 (52.6)	13,645 (60.7)	16,710 (74.3)	23,230 (103.3)	25,445 (113.2)	29,385 (130.7)	35,990 (160.1)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³Compare tabular values to the steel values in Table 4. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.

⁴Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁵Tabular values are for dry and water saturated concrete conditions.

⁶Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.

⁷Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: For sand-lightweight, $\lambda_a = 0.51$. For all-lightweight, $\lambda_a = 0.45$.

⁸Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tabular values in tension and shear by $\alpha_{seis} = 0.75$. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Table 4. Steel design strength for Hilti KH-EZ / KH-EZ CRC anchors^{1,2}

Nominal anchor diameter in.	Tensile ³ ϕN_{sa} lb (kN)	Shear ⁴ ϕV_{sa} lb (kN)	Seismic Shear ⁵ ϕV_{sa} lb (kN)
3/8	6,720 (29.9)	3,110 (13.8)	1,865 (8.3)
1/2	11,780 (52.4)	5,545 (24.7)	3,330 (14.8)
5/8	15,735 (70.0)	6,735 (30.0)	4,040 (18.0)
3/4	20,810 (92.6)	9,995 (44.5)	6,935 (30.8)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Hilti KH-EZ / KH-EZ CRC anchors are to be considered brittle steel elements.

³Tensile $\phi N_{sa} = \phi A_{se,N} f_{uta}$ as noted in ACI 318 Chapter 17.

⁴Shear values determined by static shear tests with $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$ as noted in ACI 318 Chapter 17.

⁵Seismic shear values determined by seismic shear tests with $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$ as noted in ACI 318 Chapter 17. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Figure 3. Hilti Kwik-X Dual Action SS316 Anchor installation conditions

Permissible Base Material	Dry concrete		Permissible Drilling Method	Hammer drilling with carbide tipped drill bit	
	Uncracked concrete			Hilti TE-CD or TE-YD hollow drill bit (except 3/8" diameter)	
Permissible Base Material	Water-saturated concrete		Permissible Drilling Method	Diamond core drill bit (except 3/8" diameter)	
	Cracked concrete				

Table 5. Hilti Kwik-X Dual Action SS316 anchor installation specifications

Design information		Symbol	Units	Nominal anchor diameter (in.)	
				3/8	1/2
Drill hole diameter		d_o	in.	3/8	1/2
Minimum fixture hole diameter		d_f	in.	1/2	5/8
Nominal embedment ¹		h_{nom}	in. (mm)	2-1/2 – 3 (64 – 76)	3 – 4-1/4 (76 – 108)
KHC Capsule size		-	-	3/8" Small	1/2" Small
Drilled hole depth ²	Hole condition 1	h_1	in. (mm)	N/A	
	Hole condition 2	h_1	in. (mm)	$h_{nom} + 3/8$ ($h_{nom} + 10$)	$h_{nom} + 3/8$ ($h_{nom} + 10$)
Minimum anchor spacing		s_{min}	in. (mm)	3 (76)	3 (76)
Minimum edge distance		c_{min}	in. (mm)	1-1/2 (38)	1-3/4 (44)
Minimum concrete thickness		h_{min}	in. (mm)	$h_1 + 1-1/4$ ($h_1 + 32$)	$h_1 + 1-1/4$ ($h_1 + 32$)

¹Nominal embedment (h_{nom}) = effective embedment (h_{ef}).

²See Figure 2 for description of drilled hole conditions.

Table 6. Steel Design Strength for Hilti KH-EZ SS316 Anchors^{1,2,3}

Anchor Diameter in.	Tensile ⁴ ϕN_{sa} lb (kN)	Shear ⁵ ϕV_{sa} lb (kN)	Seismic Shear ⁶ ϕV_{sa} lb (kN)
3/8	9,820 (43.7)	2,830 (12.6)	2,830 (12.6)
1/2	15,490 (68.9)	3,115 (13.9)	3,115 (13.9)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Hilti KH-EZ SS316 anchors are to be considered ductile steel elements.

³Tensile $\phi N_{sa} = \phi A_{se,N} f_{uta}$ as noted in ACI 318 Chapter 17.

⁴Shear values determined by static shear tests with $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$ as noted in ACI 318 Chapter 17.

⁵Seismic shear values determined by seismic shear tests with $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$ as noted in ACI 318 Chapter 17.

⁶See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Table 7. Hilti Kwik-X Dual Action SS316 anchor design strength with concrete / bond failure in uncracked concrete^{1,2,3,4,5,6,7,8}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - ϕN_n				Shear - ϕV_n			
		$f'_c = 2500$ psi (17.2 Mpa) lb (kN)	$f'_c = 3000$ psi (20.7 Mpa) lb (kN)	$f'_c = 4000$ psi (27.6 Mpa) lb (kN)	$f'_c = 6000$ psi (41.4 Mpa) lb (kN)	$f'_c = 2500$ psi (17.2 Mpa) lb (kN)	$f'_c = 3000$ psi (20.7 Mpa) lb (kN)	$f'_c = 4000$ psi (27.6 Mpa) lb (kN)	$f'_c = 6000$ psi (41.4 Mpa) lb (kN)
3/8	2-1/2 (64)	3,085 (13.7)	3,375 (15.0)	3,900 (17.3)	4,725 (21.0)	6,640 (29.5)	7,275 (32.4)	8,400 (37.4)	10,180 (45.3)
	3-1/4 (83)	4,405 (19.6)	4,720 (21.0)	5,265 (23.4)	6,145 (27.3)	9,490 (42.2)	10,170 (45.2)	11,345 (50.5)	13,235 (58.9)
1/2 ⁹	3 (76)	4,055 (18.0)	4,440 (19.8)	5,125 (22.8)	6,280 (27.9)	8,730 (38.8)	9,565 (42.5)	11,040 (49.1)	13,525 (60.2)
	4-1/4 (108)	5,925 (26.4)	6,490 (28.9)	7,490 (33.3)	9,175 (40.8)	12,760 (56.8)	13,975 (62.2)	16,135 (71.8)	19,765 (87.9)

Table 8. Hilti Kwik-X Dual Action SS316 anchor design strength with concrete / bond failure in cracked concrete^{1,2,3,4,5,6,7,8,9}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - ϕN_n				Shear - ϕV_n			
		$f'_c = 2500$ psi (17.2 Mpa) lb (kN)	$f'_c = 3000$ psi (20.7 Mpa) lb (kN)	$f'_c = 4000$ psi (27.6 Mpa) lb (kN)	$f'_c = 6000$ psi (41.4 Mpa) lb (kN)	$f'_c = 2500$ psi (17.2 Mpa) lb (kN)	$f'_c = 3000$ psi (20.7 Mpa) lb (kN)	$f'_c = 4000$ psi (27.6 Mpa) lb (kN)	$f'_c = 6000$ psi (41.4 Mpa) lb (kN)
3/8	2-1/2 (64)	1,665 (7.4)	1,760 (7.8)	1,925 (8.6)	2,185 (9.7)	3,585 (15.9)	3,795 (16.9)	4,150 (18.5)	4,705 (20.9)
	3-1/4 (83)	3,200 (14.2)	3,385 (15.1)	3,700 (16.5)	4,195 (18.7)	6,890 (30.6)	7,290 (32.4)	7,970 (35.5)	9,035 (40.2)
1/2 ⁹	3 (76)	2,870 (12.8)	3,145 (14.0)	3,630 (16.1)	4,450 (19.8)	6,185 (27.5)	6,775 (30.1)	7,820 (34.8)	9,580 (42.6)
	4-1/4 (108)	4,840 (21.5)	5,305 (23.6)	6,125 (27.2)	7,500 (33.4)	10,425 (46.4)	11,420 (50.8)	13,190 (58.7)	16,150 (71.8)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³Compare tabular values to the steel values in Table 6. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.

⁴Data is for temperature range A: Max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). For temperature range B: Max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C) multiply above values by 0.98. Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁵Tabular values are for dry and water saturated concrete conditions.

⁶Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.

⁷Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows:

⁸For sand-lightweight, $\lambda_a = 0.51$. For all-lightweight, $\lambda_a = 0.45$.

⁹Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tabular values in tension and shear by $a_{seis} = 0.75$. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

The Kwik-X Dual Action Anchor system will provide greater load capacities with greater flexibility. This includes immediate loading in a vast range of temperatures. The amount of load capacity immediately available after installation of the Kwik-X Dual Action Anchor system will vary depending on the concrete temperature at the time of installation. As shown in Figure 3 below, in the very cold spectrum of temperatures the immediate load capacity available will be that of the Hilti KH-EZ / KH-EZ CRC KH-EZ SS316 screw anchor until the full cure time has elapsed. For the load capacity of the Hilti KH-EZ / KH-EZ CRC / KH-EZ SS316 screw anchor please refer to ESR-3027 or Section 3.3.6 or 3.3.7 of PTG Ed. 22.

Figure 4. Cure time and immediate load allowance

 °C °F		 °C °F		 $t_{cure,full}$
-28 ... -10	-18 ... 14	5 ... 40	41 ... 104	24 h
-10 ... 5	14 ... 41	5 ... 40	41 ... 104	30 min
5 ... 40	41 ... 104	5 ... 40	41 ... 104	0.5 min

 $t \geq t_{cure,full}$	 ↓ Kwik-X ↓
 $t < t_{cure,full}$	 ↓ KH-EZ ↓

Design Data in Concrete per CSA A23.3

CSA A23.3 Annex D Design

This section contains the Limit State Design tables with un-factored characteristic loads and pre-calculated factored resistance tables based on the published loads in ICC Evaluation Services ESR-5065 and testing per ACI 355.4.

For a detailed explanation of the tables developed in accordance with CSA A23.3 Annex D, refer to Sections 3.1.7 and 3.1.8 of the 2022 PTG Ed. 22. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at www.hilti.ca.

Table 9. Hilti Kwik-X Dual Action Carbon Steel Anchor design information in hammer drilled and/or core drilled holes in accordance with CSA A23.3 Annex D¹

Design Parameter		Symbol	Units	KH-EZ/KH-EZ CRC Anchor diameter (in.)				Ref A23.3	
				3/8		1/2	5/8		3/4
Nominal anchor diameter		d _a	mm	9.5		12.7	15.9	19.1	
Effective minimum embedment ²		h _{ef,min}	mm	64	76	76	83	102	
Effective maximum embedment ²		h _{ef,max}	mm	76	114	140	152	184	
Minimum concrete thickness ²		h _{min}	mm	See Table1 and Figure 2 of this document					
Critical edge distance		c _{ac}	-	See ESR-5065, section 4.1.10					
Minimum edge distance		c _{min}	mm	38		44	44	44	
Minimum anchor spacing		s _{min}	mm	76		76	102	102	
Coeff. for factored concrete breakout resistance, uncracked concrete		k _{c,uncr} ³	-	10					D.6.2.2
Coeff. for factored concrete breakout resistance, cracked concrete		k _{c,cr} ³	-	7					D.6.2.2
Concrete material resistance factor		ϕ _c	-	0.65					8.4.2
Resistance modification factor fortension and shear, concrete failure modes, Condition B4		R _{conc}	-	100					D.5.3(c)
Minimum specified ultimate strength		f _{uta}	psi (N/mm ²)	120,300 (829)		112,540 (776)	90,180 (622)	81,600 (563)	
Effective tensile stress area		A _{se,N}	in ² (mm ²)	0.086 (55.5)		0.161 (103.9)	0.268 (172.9)	0.392 (252.9)	
Steel embedment material resistance factor for reinforcement		ϕ _s	-	0.85					8.4.3
Resistance modification factor for tension, steel failure modes ⁴		R	-	0.70					D.5.3
Resistance modification factor for shear, steel failure modes ⁴		R	-	0.65					D.5.3
Factored steel resistance intension		N _{sar}	lb (kN)	6,150 (27.4)		10,780 (48.0)	14,405 (64.1)	19,050 (84.7)	D.6.1.2
Effective tensile stress area		V _{sar}	lb (kN)	2,865 (12.7)		5,110 (22.7)	6,200 (64.1)	9,205 (40.9)	D.7.1.2
Effective tensile stress area		V _{sar,eq}	lb (kN)	1,720 (7.7)		3,065 (13.6)	3,720 (16.5)	6,385 (28.4)	
Temperature Range ⁵	Characteristic bond stress in cracked concrete ⁶	τ _{cr}	psi (MPa)	1,045 (7.2)	2,000 (13.8)	1,900 (13.1)	1,800 (12.4)	1,700 (11.7)	D.6.5.2
	Characteristic bond stress in uncracked concrete ⁶	τ _{uncr}	psi (MPa)	2,235 (15.4)		2,125 (14.7)	2,020 (13.9)	1,915 (13.2)	D.6.5.2
Reduction for seismic tension		α _{N,seis}	-	1.00					
Permissible installation conditions	Resistance modification factor tension and shear, bond failure dry and water saturated concrete	Anchor category	-	1					D.5.3(c)
		R _{dry,ws}	-	1.00					

¹Design information in this table is taken from ICC-ES ESR-5065 and converted for use with CSA A23.3 Annex D.

²See Table 1 and Figure 2 of this document.

³For all design cases, $\psi_{c,N} = 1.0$. The appropriate coefficient for breakout resistance for cracked concrete ($k_{c,cr}$) or uncracked concrete ($k_{c,uncr}$) must be used.

⁴For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.

⁵Temperature range A: Max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). Temperature range B: Max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁶Bond strength values corresponding to concrete compressive strength $f'_c = 2,500$ psi (17.2 MPa). For concrete compressive strength, f'_c , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of $(f'_c/2,500)^n$ [for SI: $(f'_c/17.2)^n$] where n is as follows: n = 0.38 and n = 0.50 for 3/8" and 1/2" respectively, in uncracked concrete, hammer drilling with carbide bit; n = 0.31 and n = 0.39 for 3/8" and 1/2" respectively, in cracked concrete, hammer drilling with carbide bit; n = 0.50 for 1/2" in uncracked and cracked concrete, diamond core bit drilling

Table 10. Hilti Kwik-X Dual Action Carbon Steel anchor factored resistance with concrete / bond failure in uncracked concrete^{1,2,3,4,5,6,7,8,9}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - Nr				Shear - Vr			
		f _c = 20 MPa (2,900 psi) lb (kN)	f _c = 25 MPa (3,625 psi) lb (kN)	f _c = 30 MPa (4,350 psi) lb (kN)	f _c = 40 MPa (5,800 psi) lb (kN)	f _c = 20 MPa (2,900 psi) lb (kN)	f _c = 25 MPa (3,625 psi) lb (kN)	f _c = 30 MPa (4,350 psi) lb (kN)	f _c = 40 MPa (5,800 psi) lb (kN)
3/8	2-1/2 (64)	3,305 (14.7)	3,695 (16.4)	4,050 (18.0)	4,675 (20.8)	6,615 (29.4)	7,395 (32.9)	8,100 (36.0)	9,355 (41.6)
	3-1/4 (83)	4,900 (21.8)	5,480 (24.4)	6,005 (26.7)	6,475 (28.8)	9,805 (43.6)	10,960 (48.8)	12,005 (53.4)	12,950 (57.6)
	4-1/2 (114)	7,910 (35.2)	8,235 (36.6)	8,510 (37.9)	8,965 (39.9)	15,825 (70.4)	16,475 (73.3)	17,025 (75.7)	17,930 (79.7)
1/2	3 (76)	4,345 (19.3)	4,860 (21.6)	5,325 (23.7)	6,145 (27.3)	8,695 (38.7)	9,720 (43.2)	10,650 (47.4)	12,295 (54.7)
	4-1/4 (108)	7,330 (32.6)	8,195 (36.5)	8,975 (39.9)	10,365 (46.1)	14,660 (65.2)	16,390 (72.9)	17,955 (79.9)	20,730 (92.2)
	5-1/2 (140)	10,790 (48.0)	12,065 (53.7)	13,190 (58.7)	13,890 (61.8)	21,580 (96.0)	24,130 (107.3)	26,375 (117.3)	27,780 (123.6)
5/8	3-1/4 (83)	4,900 (21.8)	5,480 (24.4)	6,005 (26.7)	6,930 (30.8)	9,805 (43.6)	10,960 (48.8)	12,005 (53.4)	13,865 (61.7)
	4 (102)	6,690 (29.8)	7,480 (33.3)	8,195 (36.5)	9,465 (42.1)	13,385 (59.5)	14,965 (66.6)	16,395 (72.9)	18,930 (84.2)
	5 (127)	9,355 (41.6)	10,455 (46.5)	11,455 (51.0)	13,225 (58.8)	18,705 (83.2)	20,915 (93.0)	22,910 (101.9)	26,455 (117.7)
	6 (152)	12,295 (54.7)	13,745 (61.1)	15,060 (67.0)	17,385 (77.3)	24,590 (109.4)	27,490 (122.3)	30,115 (134.0)	34,775 (154.7)
3/4	4 (102)	6,690 (29.8)	7,480 (33.3)	8,195 (36.5)	9,465 (42.1)	13,385 (59.5)	14,965 (66.6)	16,395 (72.9)	18,930 (84.2)
	5 (127)	9,355 (41.6)	10,455 (46.5)	11,455 (51.0)	13,225 (58.8)	18,705 (83.2)	20,915 (93.0)	22,910 (101.9)	26,455 (117.7)
	6-1/4 (159)	13,070 (58.1)	14,615 (65.0)	16,010 (71.2)	18,485 (82.2)	26,140 (116.3)	29,230 (130.0)	32,020 (142.4)	36,970 (164.5)
	7-1/4 (184)	16,330 (72.6)	18,260 (81.2)	20,000 (89.0)	23,095 (102.7)	32,660 (145.3)	36,515 (162.4)	40,000 (177.9)	46,190 (205.5)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³Compare tabular values to the steel values in Table 12. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.

⁴Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C).

⁵Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁶Tabular values are for dry and water saturated concrete conditions.

⁷Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.

⁸Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: For sand-lightweight, $\lambda_a = 0.51$. For all-lightweight, $\lambda_a = 0.45$.

⁹Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete.

Table 11. Hilti Kwik-X Dual Action Carbon Steel anchor factored resistance with concrete / bond failure in cracked concrete^{1,2,3,4,5,6,7,8}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - N_r				Shear - V_r			
		$f'_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f'_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f'_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f'_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f'_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f'_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f'_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f'_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	2,045 (9.1)	2,110 (9.4)	2,160 (9.6)	2,250 (10.0)	4,085 (18.2)	4,215 (18.8)	4,325 (19.2)	4,505 (20.0)
	3-1/4 (83)	3,430 (15.3)	3,835 (17.1)	4,200 (18.7)	4,850 (21.6)	6,860 (30.5)	7,670 (34.1)	8,405 (37.4)	9,705 (43.2)
	4-1/2 (114)	5,590 (24.9)	6,250 (27.8)	6,845 (30.5)	7,755 (34.5)	11,180 (49.7)	12,500 (55.6)	13,695 (60.9)	15,510 (69.0)
1/2	3 (76)	3,045 (13.5)	3,400 (15.1)	3,725 (16.6)	4,305 (19.1)	6,085 (27.1)	6,805 (30.3)	7,455 (33.2)	8,605 (38.3)
	4-1/4 (108)	5,130 (22.8)	5,735 (25.5)	6,285 (28.0)	7,255 (32.3)	10,260 (45.6)	11,475 (51.0)	12,570 (55.9)	14,510 (64.6)
	5-1/2 (140)	7,555 (33.6)	8,445 (37.6)	9,250 (41.1)	10,680 (47.5)	15,105 (67.2)	16,890 (75.1)	18,500 (82.3)	21,365 (95.0)
5/8	3-1/4 (83)	3,430 (15.3)	3,835 (17.1)	4,200 (18.7)	4,850 (21.6)	6,860 (30.5)	7,670 (34.1)	8,405 (37.4)	9,705 (43.2)
	4 (102)	4,685 (20.8)	5,240 (23.3)	5,740 (25.5)	6,625 (29.5)	9,370 (41.7)	10,475 (46.6)	11,475 (51.0)	13,250 (58.9)
	5 (127)	6,545 (29.1)	7,320 (32.6)	8,020 (35.7)	9,260 (41.2)	13,095 (58.2)	14,640 (65.1)	16,035 (71.3)	18,520 (82.4)
	6 (152)	8,605 (38.3)	9,620 (42.8)	10,540 (46.9)	12,170 (54.1)	17,215 (76.6)	19,245 (85.6)	21,080 (93.8)	24,340 (108.3)
3/4	4 (102)	4,685 (20.8)	5,240 (23.3)	5,740 (25.5)	6,625 (29.5)	9,370 (41.7)	10,475 (46.6)	11,475 (51.0)	13,250 (58.9)
	5 (127)	6,545 (29.1)	7,320 (32.6)	8,020 (35.7)	9,260 (41.2)	13,095 (58.2)	14,640 (65.1)	16,035 (71.3)	18,520 (82.4)
	6-1/4 (159)	9,150 (40.7)	10,230 (45.5)	11,205 (49.8)	12,940 (57.6)	18,300 (81.4)	20,460 (91.0)	22,410 (99.7)	25,880 (115.1)
	7-1/4 (184)	11,430 (50.8)	12,780 (56.9)	14,000 (62.3)	16,165 (71.9)	22,865 (101.7)	25,560 (113.7)	28,000 (124.6)	32,335 (143.8)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³Compare tabular values to the steel values in Table 12. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.

⁴Data is for max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁵Tabular values are for dry and water saturated concrete conditions.

⁶Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.

⁷Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: For sand-lightweight, $\lambda_a = 0.51$. For all-lightweight, $\lambda_a = 0.45$.

⁸Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tabular values in tension and shear by $a_{seis} = 0.75$. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Table 12. Steel resistance for Hilti KH-EZ / KH-EZ CRC carbon steel screw anchor^{1,2}

Nominal anchor diameter in.	Tensile ³ N_{sar} lb (kN)	Shear ⁴ V_{sar} lb (kN)	Seismic Shear ⁵ $V_{sar,eq}$ lb (kN)
3/8	6,150 (27.4)	2,865 (12.7)	1,720 (7.7)
1/2	10,780 (48.0)	5,110 (22.7)	3,065 (13.6)
5/8	14,405 (64.1)	6,200 (27.6)	3,720 (16.5)
3/4	19,050 (84.7)	9,205 (40.9)	6,385 (28.4)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Hilti KH-EZ / KH-EZ CRC carbon steel screw anchors are to be considered brittle steel elements.

³Tensile $N_{sar} = A_{se,N} \phi_s f_{uta} R$ as noted in CSA A23.3 Annex D.

⁴Shear determined by static shear tests with $V_{sar} < 0.6 A_{se,V} \phi_s f_{uta} R$ as noted in CSA A23.3 Annex D.

⁵Seismic shear values determined by seismic shear tests with $V_{sar,eq} \leq 0.60 A_{se,V} \phi_s f_{uta} R$ as noted in CSA A23.3 Annex D. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Table 13. Hilti Kwik-X Dual Action SS316 anchor design information in hammer drilled and/or core drilled holes in accordance with CSA A23.3 Annex D¹

Design parameter		Symbol	Units	Nominal anchor diameter (in.)			Ref A23.3
				3/8		1/2	
Nominal anchor diameter		d _a	mm	9.5		12.7	
Effective minimum embedment ²		h _{ef,min}	mm	64	76	76	
Effective maximum embedment ²		h _{ef,max}	mm	76	83	108	
Min. concrete thickness ²		h _{min}	mm	See Table 1 and Figure 2 of this document			
Critical edge distance		c _{ac}	-	See ESR-5065, section 4.1.10			
Minimum edge distance		c _{min}	mm	38		45	
Minimum anchor spacing		s _{min}	mm	76		76	
Coeff. for factored conc. breakout resistance, uncracked concrete		k _{c,uncr} ³	-	10.0			D.6.2.2
Coeff. for factored conc. breakout resistance, cracked concrete		k _{c,cr} ³	-	7.0			D.6.2.2
Concrete material resistance factor		ϕ _c	-	0.65			8.4.2
Resistance modification factor for tension and shear, concrete failure modes, Condition B ⁴		R _{conc}	-	1.00			D.5.3 (c)
Minimum specified ultimate strength		f _{uta}	psi (N/mm ²)	139,300 (961)		120,100 (828)	
Effective tensile stress area		A _{se,N}	in ² (mm ²)	0.094 (60.8)		0.172 (111.2)	
Steel embedment material resistance factor for reinforcement.		ϕ _s	-	0.85			8.4.3
Resistance modification factor for tension, steel failure modes ⁴		R	-	0.80			D.5.3
Resistance modification factor for shear, steel failure mode ⁴		R	-	0.75			D.5.3
Factored steel resistance in tension		N _{sar}	lb (kN)	8,905 (39.6)		14,045 (62.5)	D.6.1.2
Effective tensile stress area		V _{sar}	lb (kN)	2,775 (12.3)		3,055 (13.6)	D.7.1.2
Effective tensile stress area		V _{sar,eq}	lb (kN)	2,775 (12.3)		3,055 (13.6)	
Carbide Bit							
Temp. range A ⁵	Characteristic bond stress in cracked concrete ⁶	τ _{cr}	psi (MPa)	870 (6.0)	1,285 (8.9)	1,240 (8.6)	D.6.5.2
	Characteristic bond stress in uncracked concrete ⁶	τ _{uncr}	psi (MPa)	1,770 (12.2)		1,365 (9.4)	D.6.5.2
Temp. range B ⁵	Characteristic bond stress in cracked concrete ⁶	τ _{cr}	psi (MPa)	850 (5.9)	1,255 (8.7)	1,215 (8.4)	D.6.5.2
	Characteristic bond stress in uncracked concrete ⁶	τ _{uncr}	psi (MPa)	1,730 (11.9)		1,330 (9.2)	D.6.5.2
Reduction for seismic tension		α _{N,seis}	-	1.00			
Diamond Core Drill Bit							
Temp. range A ⁵	Characteristic bond stress in cracked concrete ⁶	τ _{cr}	psi (MPa)	N/A		1,005 (6.9)	D.6.5.2
	Characteristic bond stress in uncracked concrete ⁶	τ _{uncr}	psi (MPa)	N/A		1,295 (8.9)	D.6.5.2
Temp. range B ⁵	Characteristic bond stress in cracked concrete ^{6f}	τ _{cr}	psi (MPa)	N/A		980 (6.8)	D.6.5.2
	Characteristic bond stress in uncracked concrete ⁶	τ _{uncr}	psi (MPa)	N/A		1,265 (8.7)	D.6.5.2
Reduction for seismic tension		α _{N,seis}	-	1.00			
Carbide Bit or Diamond Core Drill Bit							
Permissible installation conditions	Resistance modification factor tension & shear, bond failure dry and water saturated concrete	Anchor category	-	1			D.5.3 (c)
		R _{dry,ws}	-	1.00			

¹Design information in this table is taken from ICC-ES ESR-5065 and converted for use with CSA A23.3 Annex D.

²See Table 1 and Figure 2 of this document.

³For all design cases, $\psi_{c,N} = 1.0$. The appropriate coefficient for breakout resistance for cracked concrete ($k_{c,cr}$) or uncracked concrete ($k_{c,uncr}$) must be used.

⁴For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.

⁵Temperature range A: Max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). Temperature range B: Max. short term temperature = 176°F (80°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁶Bond strength values corresponding to concrete compressive strength $f'_c = 2,500$ psi (17.2 MPa). For concrete compressive strength, f'_c , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of $(f'_c/2,500)^n$ [for SI: $(f'_c/17.2)^n$] where n is as follows: $n = 0.38$ and $n = 0.50$ for 3/8" and 1/2" respectively, in uncracked concrete, hammer drilling with carbide bit; $n = 0.31$ and $n = 0.39$ for 3/8" and 1/2" respectively, in cracked concrete, hammer drilling with carbide bit; $n = 0.50$ for 1/2" in uncracked and cracked concrete, diamond core bit drilling

Table 14. Hilti Kwik-X SS316 Dual Action anchor factored resistance with concrete / bond failure in uncracked concrete^{1,2,3,4,5,6,7,8}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - N_r				Shear - V_r			
		$f'_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f'_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f'_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f'_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f'_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f'_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f'_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f'_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	3,305 (14.7)	3,695 (16.4)	4,050 (18.0)	4,665 (20.8)	3,305 (14.7)	3,695 (16.4)	4,050 (18.0)	4,665 (20.8)
	3-1/4 (83)	4,660 (20.7)	5,075 (22.6)	5,440 (24.2)	6,065 (27.0)	9,325 (41.5)	10,150 (45.1)	10,875 (48.4)	12,135 (54.0)
1/2 ⁹	3 (76)	4,345 (19.3)	4,860 (21.6)	5,325 (23.7)	6,145 (27.3)	8,695 (38.7)	9,720 (43.2)	10,650 (47.4)	12,295 (54.7)
	4-1/4 (108)	6,380 (28.4)	7,135 (31.7)	7,815 (34.8)	9,025 (40.1)	12,760 (56.8)	14,270 (63.5)	15,630 (69.5)	18,050 (80.3)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

³Compare tabular values to the steel values in Table 16. The lesser of the values is to be used for the design. Tables do not consider effects of edge distance, spacing, or concrete thickness. Use Hilti PROFIS Engineering design software for designs that require additional design considerations.

⁴Data is for max. short term temperature = 130°F (54°C), max. long term temperature = 110°F (43°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

⁵Tabular values are for dry and water saturated concrete conditions.

⁶Tabular values are for short term loads only. For sustained loads including overhead use, see PTG Ed. 22 Section 3.1.8.

⁷Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: For sand-lightweight, $\lambda_a = 0.51$. For all-lightweight, $\lambda_a = 0.45$.

⁸Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tabular values in tension and shear by $\alpha_{seis} = 0.75$. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

⁹Tabular values are for holes drilled in concrete with carbide tipped hammer drill bit. For diamond core drilling with 1/2" diameter anchors only, multiply uncracked concrete tabular values by 0.95 and cracked concrete tabular values by 0.90.

Table 15. Hilti Kwik-X SS316 Dual Action anchor factored resistance with concrete / bond failure in cracked concrete^{1, 2, 3, 4, 5, 6, 7, 8}

Nominal anchor diameter in.	Effective embedment in. (mm)	Tension - N_r				Shear - V_r			
		$f'_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f'_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f'_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f'_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)	$f'_c = 20 \text{ MPa}$ (2,900 psi) lb (kN)	$f'_c = 25 \text{ MPa}$ (3,625 psi) lb (kN)	$f'_c = 30 \text{ MPa}$ (4,350 psi) lb (kN)	$f'_c = 40 \text{ MPa}$ (5,800 psi) lb (kN)
3/8	2-1/2 (64)	1,745 (7.8)	1,870 (8.3)	1,980 (8.8)	2,165 (9.6)	1,745 (7.8)	1,870 (8.3)	1,980 (8.8)	2,165 (9.6)
	3-1/4 (83)	3,350 (14.9)	3,590 (16.0)	3,800 (16.9)	4,150 (18.5)	6,700 (29.8)	7,180 (31.9)	7,595 (33.8)	8,305 (36.9)
1/2 9	3 (76)	3,045 (13.5)	3,400 (15.1)	3,725 (16.6)	4,305 (19.1)	6,085 (27.1)	6,805 (30.3)	7,455 (33.2)	8,605 (38.3)
	4-1/4 (108)	5,130 (22.82)	5,735 (25.52)	6,285 (27.95)	7,255 (32.28)	10,260 (45.64)	11,475 (51.03)	12,570 (55.90)	14,510 (64.55)

Table 16. Steel resistance for Hilti Kwik-X SS316 screw anchor^{1,2}

Nominal anchor diameter in.	Tensile ³ N_{sar} lb (kN)	Shear ⁴ V_{sar} lb (kN)	Seismic Shear ⁵ $V_{sar,eq}$ lb (kN)
3/8	7,855 (34.9)	2,450 (10.9)	2,450 (10.9)
1/2	14,045 (62.5)	3,055 (13.6)	3,055 (13.6)

¹See PTG Ed. 22 Section 3.1.8 to convert design strength value to ASD value.

²Hilti KH-EZ carbon steel screw anchors are to be considered brittle steel elements.

³Tensile $N_{sar} = A_{se,N} \phi_s f_{uta}$ R as noted in CSA A23.3 Annex D.

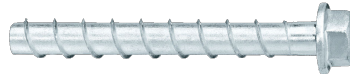
⁴Shear determined by static shear tests with $V_{sar} < 0.6 A_{se,V} \phi_s f_{uta}$ R as noted in CSA A23.3 Annex D. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

⁵Seismic shear values determined by seismic shear tests with $V_{sar,eq} < 0.60 A_{se,V} \phi_s f_{uta}$ R as noted in CSA A23.3 Annex D. See PTG Ed. 22 Section 3.1.8 for additional information on seismic applications.

Product Portfolio



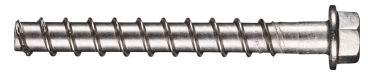
Hilti KHC Kwik-X Capsule



Hilti KH-EZ Screw Anchor



Hilti KH-EZ CRC Screw Anchor



Hilti KH-EZ SS316 Screw Anchor

Kwik-X Dual Action Anchor

Description	Hole diameter in.	Minimum Embedment	Maximum Embedment	Qty / Box
KHC Kwik-X Capsule 3/8" SMALL	3/8"	2-1/2	3	50
KHC Kwik-X Capsule 3/8" LARGE	3/8"	3	4-1/2	50
KHC Kwik-X Capsule 1/2" SMALL	1/2"	3	4-1/4	25
KHC Kwik-X Capsule 1/2" LARGE	1/2"	4-1/4	5-1/2	25
KHC Kwik-X Capsule 5/8" SMALL	5/8"	3-1/4	4-1/2	24
KHC Kwik-X Capsule 5/8" LARGE	5/8"	4-1/2	6	24
KHC Kwik-X Capsule 3/4" SMALL	3/4"	4	4-1/2	24
KHC Kwik-X Capsule 3/4" LARGE	3/4"	4-1/2	7-1/4	24

KH-EZ Screw Anchor

Description	Hole diameter in.	Minimum Embedment	Maximum Embedment	Qty / Box
KH-EZ 3/8"x3"	3/8"	2-1/2	3	50
KH-EZ 3/8"x3 1/2"	3/8"	2-1/2	3-1/2	50
KH-EZ 3/8"x4"	3/8"	2 -1/2	4	50
KH-EZ 3/8"x5"	3/8"	2-1/2	5	30
KH-EZ 1/2"x3 1/2"	1/2"	3	3-1/4	25
KH-EZ 1/2"x4"	1/2"	3	4	25
KH-EZ 1/2"x4 1/2"	1/2"	3	4 1/2	25
KH-EZ 1/2"x5"	1/2"	3	5	25
KH-EZ 1/2"x6"	1/2"	3	6	25
KH-EZ 5/8"x3 1/2"	1/2"	3	3-1/2	15
KH-EZ 5/8"x4"	5/8"	3-1/4	4	15
KH-EZ 5/8"x5 1/2"	5/8"	3-1/4	5-1/2	15
KH-EZ 5/8"x6 1/2"	5/8"	3-1/4	6-1/2	15
KH-EZ 5/8"x8"	5/8"	3-1/4	8	15
KH-EZ 3/4"x4 1/2"	3/4"	4	4-1/2	10
KH-EZ 3/4"x5 1/2"	3/4"	4	5-1/2	10
KH-EZ 3/4"x7"	3/4"	4	7	10
KH-EZ 3/4"x8"	3/4"	4	8	10
KH-EZ 3/4"x9"	3/4"	4	9	10

KH-EZ CRC Screw Anchor

Description	Hole diameter in.	Minimum Embedment	Maximum Embedment	Qty / Box
KH-EZ CRC 3/8"x3"	3/8"	2-1/2	3	50
KH-EZ CRC 3/8"x4"	3/8"	2-1/2	4	50
KH-EZ CRC 3/8"x5"	3/8"	2-1/2	5	30
KH-EZ CRC 1/2"x4"	1/2"	3	4	25
KH-EZ CRC 1/2"x5"	1/2"	3	5	25
KH-EZ CRC 1/2"x6"	1/2"	3	6	25
KH-EZ CRC 5/8"x5 1/2"	5/8"	3-1/4	5-1/2	15
KH-EZ CRC 5/8"x6 1/2"	5/8"	3-1/4	6-1/2	15
KH-EZ CRC 5/8"x8"	5/8"	3-1/4	8	15
KH-EZ CRC 3/4"x5 1/2"	3/4"	4	5-1/2	10
KH-EZ CRC 3/4"x7"	3/4"	4	7	10
KH-EZ CRC 3/4"x9"	3/4"	4	9	10

KH-EZ SS316 Screw Anchor

Description	Hole Diameter	Minimum Embedment	Maximum Embedment	Qty / Box
KH-EZ SS316 3/8"x3"	3/8"	2 1/2	3	25
KH-EZ SS316 3/8"x4"	3/8"	2 1/2	4	25
KH-EZ SS316 3/8"x5"	3/8"	2 1/2	5	25
KH-EZ SS316 1/2"x4"	1/2"	3	4	12
KH-EZ SS316 1/2"x5"	1/2"	3	5	12



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